

VARIATION OF BURNING SURFACE AREA FOR MULTITUBULAR CHARGES

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ABSTRACT

In continuation of the earlier work already published^{2,3} the variation of burning surface area for multi-tubular charges is discussed in this paper.

Introduction

The variation of the function of progressivity $\frac{S}{S_0}$ (the ratio of the burning surface area at any time to the initial burning surface area) is an important characteristic for any particular charge shape. An expression for $\frac{S}{S_0}$ can be easily obtained if the form-function i.e. the relation between z and f is known. Conversely from a knowledge of $\frac{S}{S_0}$ as a function of f , we can deduce the form-function. In any particular case, the decision as to which of the two functions $\frac{S}{S_0}$ or z has to be calculated first depends upon the relative ease with which either can be computed.

For a hepta-tubular charge, Tavernier¹ had deduced the expression for $\frac{S}{S_0}$ from that of z . For the second stage of burning it leads to very complicated differentiation since z is not known explicitly as a function of f . In fact he has expressed $\frac{S}{S_0}$ in terms of $K(w)$ and $I(w)$ both of which contain $H'(w)$. We have obtained in this paper an explicit expression for $K(w)$ without involving any differentiation and given the Tables for the same. Incidentally we have been able to find an explicit expression for $H'(w)$ also.

We have also examined the variation of $\left(\frac{S}{S_0}\right)_{max}$ both with m and ρ for tri-tubular, quadra-tubular and hepta-tubular charges. It appears that for a given shape this value in general increases both with m and ρ and the behaviour for a fixed value of m is similar for all values of ρ . The study which has been done for the above three charges should help us in finding out suitable values of m and ρ for choosing a shape of a particular type with given values of $\left(\frac{S}{S_0}\right)_{max}$.

Notations

The following notations have been used:

C = Mass of the grain.

δ = Propellant density.

d = The diameter of each hole of the grain.

D = The distance between any two holes or between any hole and the curved surface of the grain.

L = The length of the grain.

m = Ratio of the exterior diameter of the grain to the diameter of the holes.

$m > \left(1 + \frac{2}{\sqrt{3}}\right)$ for the tri-tubular charge.

$> (1 + \sqrt{2})$ for the quadra-tubular charge.

> 3 for the hepta-tubular charge.

ρ = Ratio of the length of the grain to the exterior diameter of the grain.

$\rho > \left[\frac{(m-1)\sqrt{3}-2}{2(\sqrt{3}+1)m} \right]$ for the tri-tubular charge.

$> \left[\frac{m(\sqrt{2}-1)-1}{m\sqrt{2}} \right]$ for the quadra-tubular charge.

$> \left[\frac{m-3}{4m} \right]$ for the hepta-tubular charge.

z = Fraction of the charge burnt at the instant ' t '.

f = Fraction of the initial thickness (web-size) remaining at the instant ' t '.

The function of progressivity for the first stage

In this section we shall find S from first principles without first finding S_0 . We have deduced the form-function for each

charge from the expression for $\frac{S}{S_0}$ as a function of :

(a) Tri-tubular charge.

The appearance of the end section of a grain is shown in the following figs 1, 2 and 3.

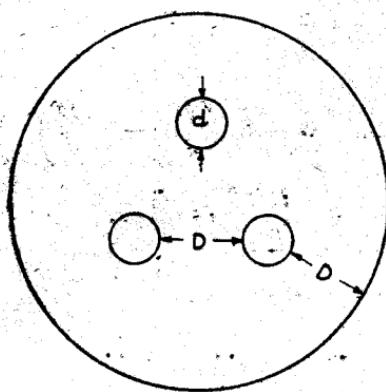


FIG 1

Unburnt position

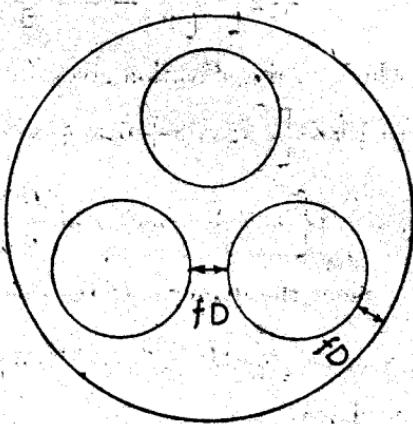


FIG 2

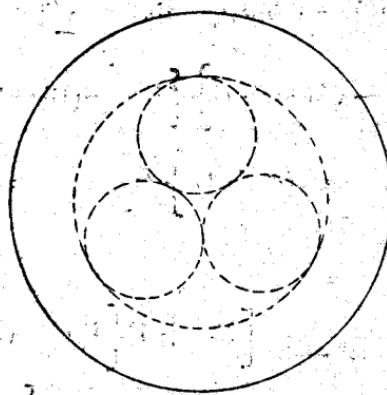
Position when a fraction f of D remains.

FIG 3

Position of the four slivers at the end of the first stage of burning

The initial surface area is given by

$$S = \left\{ 2\pi \left(\frac{md}{2} \right) + 3 \cdot 2\pi \left(\frac{d}{2} \right) \right\} \rho m d + 2 \left\{ \pi \left(\frac{md}{2} \right)^2 - 3 \pi \left(\frac{fd}{2} \right)^2 \right\}$$

$$= \frac{1}{2} \pi d^2 (2m^2 \rho + 6m \rho + m^2 - 3) \quad (1)$$

Also the surface area at any instant is given by

$$S = \left[2\pi \left\{ \left(\frac{md}{2} \right) - \frac{D(1-f)}{2} \right\} + 3.2\pi \left\{ \frac{d}{2} + \frac{D(1-f)}{2} \right\} \right] [\rho md - D(1-f)] \\ + 2 \left[\pi \left\{ \frac{md}{2} - \frac{D(1-f)}{2} \right\}^2 - 3\pi \left\{ \frac{d}{2} + \frac{D(1-f)}{2} \right\}^2 \right] \quad (2a)$$

which on simplification gives

$$S = \frac{1}{2}\pi d^2 \left[\left\{ (2m^2\rho + 6m\rho + m^2 - 3) + 4(m\rho - m - 3) \left(\frac{D}{d} \right) - 6 \left(\frac{D}{d} \right)^2 \right\} \right. \\ \left. + 4 \left\{ (m + 3 - m\rho) + 3 \left(\frac{D}{d} \right) \right\} \left(\frac{D}{d} \right) f - 6 \left(\frac{D}{d} \right)^2 f^2 \right] \quad (2b)$$

Since the diameter of the cylinder equals md i.e.

$$\frac{2}{\sqrt{3}} (D + d) + 2D + d = md \quad \dots \quad \dots \quad \dots \quad (3a)$$

we have

$$\frac{D}{d} = \frac{1}{4}[(3m - 1) - \sqrt{3}(m + 1)] \quad \dots \quad \dots \quad \dots \quad (3b)$$

Substituting for $\frac{D}{d}$ from (3b) in (2b) we get after some simplification

$$S = \frac{1}{2}\pi d^2 \left[\frac{1}{4}(m + 1) \left\{ 4(5 - \sqrt{3})m\rho - 13(2 - \sqrt{3})m + 3(3\sqrt{3} - 2) \right\} \right. \\ \left. - \frac{1}{4} \left\{ (3m - 1) - \sqrt{3}(m + 1) \right\} \left\{ 4m\rho - (13 - 3\sqrt{3})m - 3(3 - \sqrt{3}) \right\} f \right. \\ \left. - \frac{3}{8} \left\{ (3m - 1) - \sqrt{3}(m + 1) \right\}^2 f^2 \right] \quad \dots \quad \dots \quad \dots \quad (4)$$

Dividing (4) by (1)

$$\frac{S}{S_o} = \frac{1}{2m^2\rho + 6m\rho + m^2 - 3} \left[\frac{1}{4}(m + 1) \left\{ 4(5 - \sqrt{3})m\rho - 2(13m + 3) \right. \right. \\ \left. + \sqrt{3}(13m + 9) \right\} - \frac{1}{4} \left\{ (3m - 1) - \sqrt{3}(m + 1) \right\} \\ \left. \left\{ 4m\rho - (13m + 9) + 3\sqrt{3}(m + 1) \right\} f \right. \\ \left. - \frac{3}{8} \left\{ (3m - 1) - \sqrt{3}(m + 1) \right\}^2 f^2 \right] \quad \dots \quad (5a)$$

which is of the form

$$\frac{S}{S_o} = a - \beta f - \gamma f^2 \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (5b)$$

where

$$\left. \begin{aligned} a &= \frac{(m+1)[4(5 - \sqrt{3})m\rho - 2(13m + 3) + \sqrt{3}(13m + 9)]}{4(2m^2\rho + 6m\rho + m^2 - 3)} \\ \beta &= \frac{[(3m - 1) - \sqrt{3}(m + 1)][4m\rho - (13m + 9) + 3\sqrt{3}(m + 1)]}{4(2m^2\rho + 6m\rho + m^2 - 3)} \\ \gamma &= \frac{3[(3m - 1) - \sqrt{3}(m + 1)]^2}{8(2m^2\rho + 6m\rho + m^2 - 3)} \end{aligned} \right\} \quad (6)$$

(b) Quadra-tubular Charge.

The appearance of the end section of a grain is shown in the following figs. 4, 5 and 6.

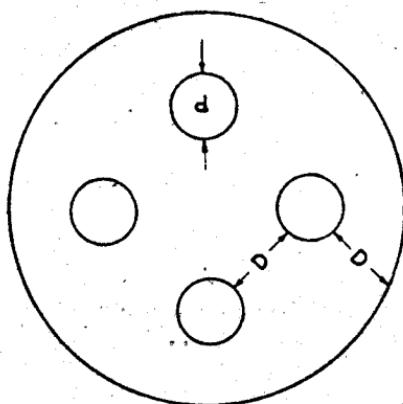


FIG 4
Unburnt position

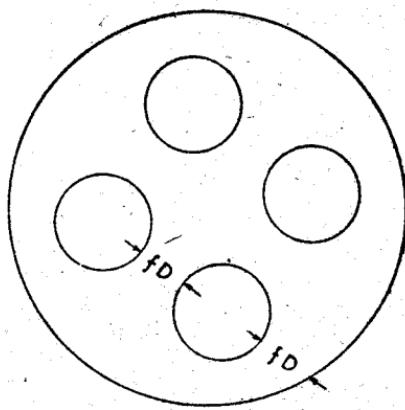


FIG 5
Position when a fraction
of D remains

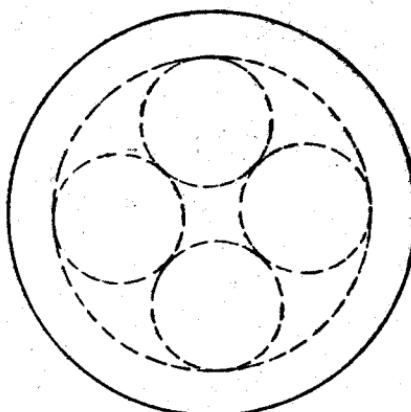


FIG 6
Position of the five slivers at the end
of the first stage of burning.

In this case

$$S_o = \left\{ 2\pi \left(\frac{md}{2} \right) + 4 \cdot 2\pi \left(\frac{d}{2} \right) \right\} \rho md + 2 \left\{ \pi \left(\frac{md}{2} \right)^2 - 4\pi \left(\frac{d}{2} \right)^2 \right\}$$

$$= \frac{1}{2}\pi d^2(2m^2\rho + 8m\rho + m^2 - 4) \quad \dots \dots \dots \quad (7)$$

Also

$$S = \left[2\pi \left\{ \left(\frac{md}{2} \right) - \frac{D(1-f)}{2} \right\} + 8\pi \left\{ \frac{df}{2} + \frac{D(1-f)}{2} \right\} \right]$$

$$\left[\rho md - D(1-f) \right] + 2 \left[\pi \left\{ \frac{md}{2} - \frac{D(1-f)}{2} \right\}^2 \right.$$

$$\left. - 3\pi \left\{ \frac{d}{2} + \frac{D(1-f)}{2} \right\}^2 \right] \quad \dots \dots \dots \quad (8a)$$

which on simplification gives

$$S = \frac{1}{2}\pi d^2 \left[\left\{ (2m^2\rho + 8m\rho + m^2 - 4) + 2(3m\rho - 2m - 8) \left(\frac{D}{d} \right) \right. \right.$$

$$\left. \left. - 9 \left(\frac{D}{d} \right)^2 \right\} + 2 \left\{ 2m + 8 - 3m\rho + 9 \left(\frac{D}{d} \right) \right\} \left(\frac{D}{d} \right) f \right.$$

$$\left. - 9 \left(\frac{D}{d} \right)^2 f^2 \right] \quad \dots \dots \dots \quad (8b)$$

Since the diameter of the cylinder equals md i.e.

$$(D+d)\sqrt{2} + d + 2D = md \quad \dots \dots \dots \quad (9a)$$

we have

$$\frac{D}{d} = \frac{m\sqrt{2} - (m+1)}{\sqrt{2}} \quad \dots \dots \dots \quad (9b)$$

Substituting for $\frac{D}{d}$ from (9b) in (8b) we obtain after a little simplification,

$$S = \frac{1}{2}\pi d^2 \left[\frac{1}{2}(m+1) \left\{ 2(8 - 3\sqrt{2})m\rho - (33m + 17) + 2\sqrt{2}(11m + 8) \right\} \right.$$

$$\left. - \left\{ m\sqrt{2} - (m+1) \right\} \left\{ 3\sqrt{2}m\rho + 9(m+1) - \sqrt{2}(11m + 8) \right\} f \right.$$

$$\left. - \frac{9}{2} \left\{ m\sqrt{2} - (m+1) \right\}^2 f^2 \right] \quad \dots \dots \dots \quad (10)$$

Dividing (10) by (7), we get

$$\frac{S}{S_o} = \frac{1}{2m^2\rho + 8m\rho + m^2 - 4} \left[\frac{1}{2}(m+1) \left\{ 2(8 - 3\sqrt{2})m\rho - (33m + 17) \right. \right.$$

$$\left. \left. + 2\sqrt{2}(11m + 8) \right\} - \left\{ m\sqrt{2} - (m+1) \right\} \right.$$

$$\left. \left\{ 3\sqrt{2}m\rho + 9(m+1) - \sqrt{2}(11m + 8) \right\} f \right]$$

$$+ \frac{9}{2} \left\{ m\sqrt{2} - (m+1) \right\}^2 f^2 \quad \dots \dots \dots \quad (11a)$$

which is of the form

$$\frac{S}{S_0} = a + \beta f - \gamma f^2 \quad (11b)$$

where

$$\left. \begin{aligned} a &= \frac{(m+1)[2(8 - 3\sqrt{2})mp - (33m + 17) + 2\sqrt{2}(11m + 8)]}{2(2m^2\rho + 8mp + m^2 - 4)} \\ \beta &= \frac{[m\sqrt{2} - (m+1)][3\sqrt{2}mp + 9(m+1) - \sqrt{2}(11m + 8)]}{(2m^2\rho + 8mp + m^2 - 4)} \\ \gamma &= \frac{9[m\sqrt{2} - (m+1)]^2}{2(2m^2\rho + 8mp + m^2 - 4)} \end{aligned} \right\} \quad (12)$$

(c) Hepta-tubular charge:

The appearance of the end section of a grain is shown in the following figs 7, 8 and 9.

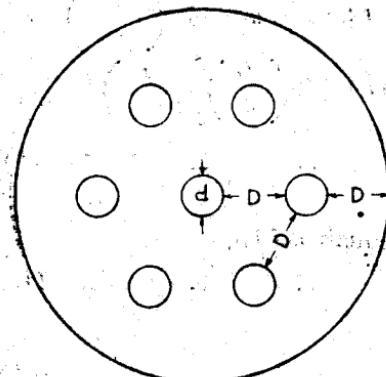


FIG 7

Unburnt position

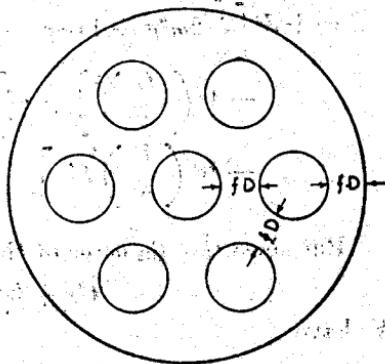


FIG 8

Position when a fraction f of D remains.

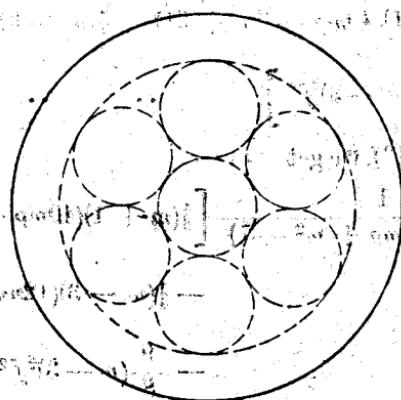


FIG 9

Position of the twelve slivers at the end
of the first stage of burning.

In this case

$$\begin{aligned} S_o &= \left[\left\{ 2\pi \left(\frac{md}{2} \right) + 14\pi \left(\frac{d}{2} \right) \right\} \rho md + 2 \left\{ \pi \left(\frac{md}{2} \right)^2 - 7\pi \left(\frac{d}{2} \right)^2 \right\} \right] \\ &= \frac{1}{2}\pi d^2(2m^2\rho + 14m\rho + m^2 - 7) \quad \dots \quad \dots \quad \dots \quad \dots \quad (13) \end{aligned}$$

Also

$$\begin{aligned} S &= \left[2\pi \left\{ \left(\frac{md}{2} \right) - \frac{D(1-f)}{2} \right\} + 14\pi \left\{ \frac{d}{2} + \frac{D(1-f)}{2} \right\} \right] \left[\rho md \right. \\ &\quad \left. - D(1-f) \right] + 2 \left[\pi \left\{ \left(\frac{md}{2} \right) - \frac{D(1-f)}{2} \right\}^2 - 7\pi \left\{ \frac{d}{2} + \right. \right. \\ &\quad \left. \left. \frac{D(1-f)}{2} \right\}^2 \right] \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (14a) \end{aligned}$$

which on simplification gives

$$\begin{aligned} S &= \frac{1}{2}\pi d^2 \left[\left\{ (2m^2\rho + 14m\rho + m^2 - 7) + 4(3m\rho - m - 7) \left(\frac{D}{d} \right) \right. \right. \\ &\quad \left. \left. - 18 \left(\frac{D}{d} \right)^2 \right\} + 4 \left\{ m + 7 - 3m\rho + 9 \left(\frac{D}{d} \right) \right\} \left(\frac{D}{d} \right) f \right. \\ &\quad \left. - 18 \left(\frac{D}{d} \right)^2 f^2 \right] \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (14b) \end{aligned}$$

But since the diameter of the cylinder equals md i.e.

$$4D + 3d = md \quad \dots \quad \dots \quad \dots \quad \dots \quad (15a)$$

We have

$$\frac{D}{d} = \frac{m-3}{4} \quad \dots \quad \dots \quad \dots \quad \dots \quad (15b)$$

Substituting for $\frac{D}{d}$ from (15b), in (14b), we obtain after simplification,

$$\begin{aligned} S &= \frac{1}{2}\pi d^2 \left[\frac{1}{8}(m+1)(40m\rho - 9m + 31) - \frac{1}{4}(m-3)(12m\rho - 13m - 1)f \right. \\ &\quad \left. - \frac{9}{8}(m-3)^2 f^2 \right] \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (16) \end{aligned}$$

Dividing (16) by (13), we get

$$\begin{aligned} \frac{S}{S_o} &= \frac{1}{(2m^2\rho + 14m\rho + m^2 - 7)} \left[\frac{1}{8}(m+1)(40m\rho - 9m + 31) \right. \\ &\quad \left. - \frac{1}{4}(m-3)(12m\rho - 13m - 1)f \right. \\ &\quad \left. - \frac{9}{8}(m-3)^2 f^2 \right] \quad \dots \quad \dots \quad (17a) \end{aligned}$$

which is of the form

$$\frac{S}{S_o} = \alpha - \beta f - \gamma f^2 \quad \dots \quad \dots \quad \dots \quad \dots \quad (17b)$$

where

$$\left. \begin{aligned} a &= \frac{(m+1)(40mp - 9m + 31)}{8(2m^2\rho + 14m\rho + m^2 - 7)} \\ \beta &= \frac{(m-3)(12mp - 13m - 1)}{4(2m^2\rho + 14m\rho + m^2 - 7)} \\ \gamma &= \frac{9}{8} \frac{(m-3)^2}{(2m^2\rho + 14m\rho + m^2 - 7)} \end{aligned} \right\} \quad (18)$$

We shall now obtain the (z, f) relation for the three charges. Since S is clearly proportional to $\frac{dz}{df}$ and since initially $S=S_0$ when $f=1$ we have,

$$\frac{S}{S_0} = \frac{\frac{dz}{df}}{\left[\frac{dz}{df} \right]_{f=1}} \quad (19a)$$

Also

$$\frac{S}{S_0} = a - \beta f - \gamma f^2 \quad (19b)$$

Hence

$$\frac{dz}{df} = K(a - \beta f - \gamma f^2) \quad (20)$$

where

$$K = \left[\frac{dz}{df} \right]_{f=1} \quad (21)$$

Integrating (20) and using the condition that initially $z=0$ when $f=1$, we obtain

$$\begin{aligned} z &= -K \left[a(1-f) - \frac{\beta}{2}(1-f^2) - \frac{\gamma}{3}(1-f^3) \right] \\ &= -K(1-f) \left[(a - \frac{1}{2}\beta - \frac{1}{3}\gamma) - (\frac{1}{2}\beta + \frac{1}{3}\gamma)f - \frac{1}{3}\gamma f^2 \right] \end{aligned} \quad (22a)$$

which is the (z, f) relation of the form

$$z = (1-f)(a - bf - cf^2) \quad (22b)$$

where

$$\left. \begin{aligned} a &= -K(a - \frac{1}{2}\beta - \frac{1}{3}\gamma) \\ b &= -K(\frac{1}{2}\beta + \frac{1}{3}\gamma) \\ c &= -K(\frac{1}{3}\gamma) \end{aligned} \right\} \quad (23)$$

We shall now obtain the value of K ($= \left[\frac{dz}{df} \right]_{f=1}$) from the equation of burning viz.

$$c(dz) = -S_0 \frac{D}{2} (df) \delta \quad (24a)$$

whence

$$\left[\frac{dz}{df} \right]_{f=1} = -\frac{D S_o \delta}{2c} = -\frac{D S_o}{2 V_o} \quad \dots \quad (24b)$$

where V_o is original volume of the grain and can be calculated for each charge. In fact

$$V_o = \left[\pi \left(\frac{m d}{2} \right)^2 - n \pi \left(\frac{d}{2} \right)^2 \right] \rho m d$$

$$= \frac{1}{4} \pi \rho m d^3 (m^2 - n) \quad \dots \quad \dots \quad \dots \quad (25)$$

where $n=3, 4$ and 7 for the tri-tubular, quadra-tubular and hepta-tubular charges respectively.

Substituting the values of D, S_o , and V_o for the three charges, we obtain the corresponding values of K for the three charges. Thus

$$K = -\frac{(2m^2\rho + 6mp + m^2 - 3)}{4mp(m^2 - 3)} \left[(3m - 1) - \sqrt{3(m+1)} \right] \text{ for the tri-tubular charge.}$$

$$= -\frac{(2m^2\rho + 8mp + m^2 - 4)}{\sqrt{2}mp(m^2 - 4)} \left[m\sqrt{2} - (m+1) \right] \text{ for the quadra-tubular charge.}$$

$$= -\frac{(2m^2\rho + 14mp + m^2 - 7)}{4mp(m^2 - 7)} \left[m - 3 \right] \text{ for the hepta-tubular charge.}$$

Now substituting the values of a, b, γ and K for the three charges we obtain, after some simplification, the corresponding expressions for a, b, c and consequently the $(z-f)$ relation

$$z = (1-f)(a - bf - cf^2) \quad \dots \quad \dots \quad \dots \quad (26)$$

for the three charges. Thus

for the tri-tubular charge;

$$a = \frac{[(3m-1)-\sqrt{3}(m+1)]}{8mp(m^2-3)} \left[(7-\sqrt{3})m^2\rho + (11-\sqrt{3})mp + 2(5\sqrt{3}-8)\left(\frac{m+1}{2}\right)^2 \right] \quad \quad \quad (27)$$

$$b = \frac{[(3m-1)-\sqrt{3}(m+1)]^2}{16mp(m^2-3)} \left[2mp - (5-\sqrt{3})(m+1) \right] \quad \quad \quad (27)$$

$$c = \frac{[(3m-1)-\sqrt{3}(m+1)]^3}{32mp(m^2-3)} \quad \quad \quad (27)$$

for the quadra-tubular charge;

$$a = \frac{[m\sqrt{2}-(m+1)]}{2\sqrt{2}mp(m^2-4)} \left[(10-3\sqrt{2})m^2\rho + (16-3\sqrt{2})mp + (8\sqrt{2}-11)(m+1)^2 \right] \quad \quad \quad (28)$$

$$b = \frac{[m\sqrt{2}-(m+1)]^2}{2mp(m^2-4)} \left[3mp - (8-3\sqrt{2})(m+1) \right] \quad \quad \quad (28)$$

$$c = \frac{3[m\sqrt{2}-(m+1)]^3}{2\sqrt{2}mp(m^2-4)} \quad \quad \quad (28)$$

and for the hepta-tubular charge:

$$\left. \begin{aligned} a &= \frac{(m-3)}{8mp(m^2-7)} \left[7m^2\rho + 19m\rho + 3\left(\frac{m+1}{2}\right)^2 \right] \\ b &= \frac{(m-3)^2}{16mp(m^2-7)} \left[6m\rho - 5m - 5 \right] \\ c &= \frac{3(m-3)^3}{32mp(m^2-7)} \end{aligned} \right\} \quad (29)$$

The function of progressivity for the second stage

(a) Tri-tubular charge:²

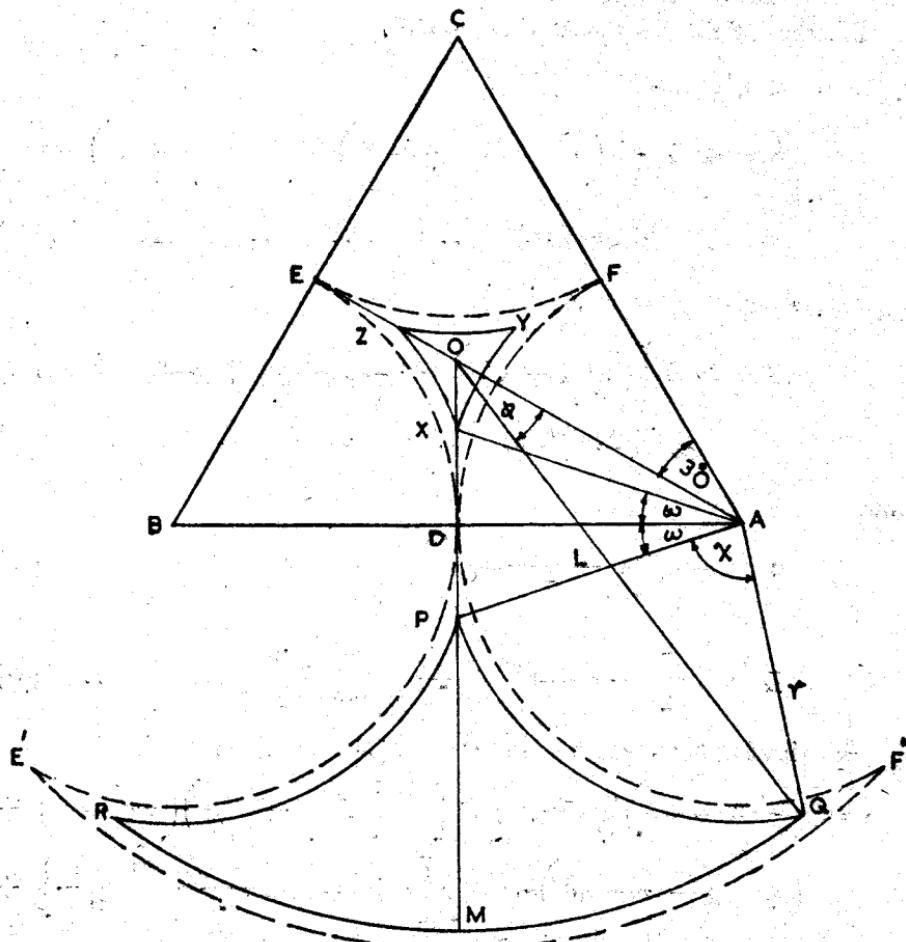


FIG 10

Length of the circumference of the $\triangle PQR$ is

$$\begin{aligned} &= 2r\chi + \frac{a}{\sqrt{3}} \left\{ 2(1 + \sqrt{3}) - \sqrt{3} \sec \omega \right\} (120^\circ - 2\phi) \\ &= 2a \left[\frac{2}{\sqrt{3}} (1 + \sqrt{3}) (60^\circ - \phi) + (\phi + \chi - 60^\circ) \sec \omega \right] \quad (30) \end{aligned}$$

and that of XYZ is

$$\begin{aligned} &= 3r(60^\circ - 2\omega) \\ &= 6a(30^\circ - \omega) \sec \omega \quad \dots \quad \dots \quad \dots \quad \dots \quad (31) \end{aligned}$$

Now the surface of the combustion at the instant ' t ' is given by

$S =$ (thrice the length of the circumference of the $\triangle PQR$ + that of the $\triangle XYZ$) \times height of the grain + twice (thrice the area of the $\triangle PQR$ + that of the $\triangle XYZ$)

But the $\triangle XYZ$ disappears when $\omega = 30^\circ$.

\therefore for $0^\circ \leq \omega \leq 30^\circ$

$$\begin{aligned} S &= 6aL \left\{ \frac{2}{\sqrt{3}} (1 + \sqrt{3}) (60^\circ - \phi) + (\phi + \chi - \omega - 30^\circ) \sec \omega \right\} \\ &\quad + 2a^2 H(\omega) \quad \dots \quad \dots \quad \dots \quad \dots \quad (32a) \end{aligned}$$

and for $30^\circ \leq \omega \leq 47^\circ 35'$

$$\begin{aligned} S &= 6aL \left\{ \frac{2}{\sqrt{3}} (1 + \sqrt{3}) (60^\circ - \varphi) + (\varphi + \chi - 60^\circ) \sec \omega \right\} \\ &\quad + 2a^2 H(\omega) \quad \dots \quad \dots \quad \dots \quad \dots \quad (32b) \end{aligned}$$

Now

$$a = (3 - \sqrt{3}) \left(\frac{m+1}{8} \right) d \quad \dots \quad \dots \quad \dots \quad \dots \quad (33)$$

and

$$L = d \left[1 + \rho m - \left(\frac{3 - \sqrt{3}}{4} \right) \frac{m+1}{\cos \omega} \right] \quad \dots \quad \dots \quad (34)$$

Substituting for a and L from (33) and (34) in (32) we obtain,

$$\begin{aligned} S &= \frac{1}{8} (3 - \sqrt{3}) (m+1) d^2 \left[6 \left\{ 2 \left(1 + \frac{1}{\sqrt{3}} \right) (60^\circ - \varphi) + (\varphi + \chi - \omega - 30^\circ) \sec \omega \right\} \left\{ 1 + m\rho - \frac{3 - \sqrt{3}}{4} \frac{m+1}{\cos \omega} \right\} + \right. \\ &\quad \left. \frac{3 - \sqrt{3}}{4} (m+1) H(\omega) \right] \quad 0^\circ \leq \omega \leq 30^\circ \quad \dots \quad \dots \quad (35a) \end{aligned}$$

and

$$S = \frac{1}{8} (3 - \sqrt{3}) (m + 1) d^2 \left[6 \left\{ 2 \left(1 + \frac{1}{\sqrt{3}} \right) (60^\circ - \varphi) + (\varphi + \chi - 60^\circ) \sec \omega \right\} \left\{ 1 + m\rho - \frac{3 - \sqrt{3}}{4} \frac{m + 1}{\cos \omega} \right\} + \frac{3 - \sqrt{3}}{4} (m+1) H(\omega) \right] \quad 30^\circ \leq \omega \leq 47^\circ 35' \quad \dots \quad (35b)$$

Also the surface of the powder initially exposed to the combustion is given by

$$S_0 = \frac{1}{2} \pi d^2 (2 m^2 \rho + 6 m \rho + m^2 - 3) \quad \dots \quad \dots \quad (36)$$

Dividing (35) by (36), we obtain

For $0^\circ \leq \omega \leq 30^\circ$,

$$\frac{S}{S_0} = \frac{(3 - \sqrt{3}) (m + 1)}{16 \pi (2m^2 \rho + 6m \rho + m^2 - 3)} \left[6 \left\{ 2 \left(1 + \frac{1}{\sqrt{3}} \right) (60^\circ - \varphi) + (\varphi + \chi - \omega - 30^\circ) \sec \omega \right\} \left\{ 4 + 4 m \rho - (3 - \sqrt{3}) \left(\frac{m + 1}{\cos \omega} \right) \right\} + (3 - \sqrt{3}) (m + 1) H(\omega) \right] \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (37a)$$

and for $30^\circ \leq \omega \leq 47^\circ 35'$,

$$\frac{S}{S_0} = \frac{(3 - \sqrt{3}) (m + 1)}{16 \pi (2m^2 \rho + 6m \rho + m^2 - 3)} \left[6 \left\{ 2 \left(1 + \frac{1}{\sqrt{3}} \right) (60^\circ - \varphi) + (\varphi + \chi - 60^\circ) \sec \omega \right\} \left\{ 4 + 4 m \rho - (3 - \sqrt{3}) \frac{m + 1}{\cos \omega} \right\} + (3 - \sqrt{3}) (m + 1) H(\omega) \right] \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (37b)$$

When $\omega = 0^\circ$, (37a) gives

$$\frac{S}{S_0} = \frac{(3 - \sqrt{3}) (m + 1)}{24 (2m^2 \rho + 6m \rho + m^2 - 3)} \left[6 \left(2 + \frac{1}{\sqrt{3}} \right) \left\{ 4 + 4 m \rho - (3 - \sqrt{3}) (m + 1) \right\} + (7\sqrt{3} - 9)(m + 1) \right]$$

which can be put in the form

$$\frac{S}{S_0} = \frac{m + 1}{4(2m^2 \rho + 6m \rho + m^2 - 3)} \left[4 (5 - \sqrt{3}) m \rho - 2 (13m + 3) + \sqrt{3} (13m + 9) \right]$$

This is the value of α at the end of the first period of burning.

The values of $\frac{S}{S_0}$ as given from (37) are tabulated below for different values of ω ranging from 0° to $47^\circ 35'$, for some set of values of m and p .

TABLE 1

m	p	0°	5°	10°	15°	20°	25°	30°	$32^\circ 30'$	35°	$37^\circ 30'$	40°	$42^\circ 30'$	45°	$47^\circ 35'$
$\frac{1}{2}$		0.665	0.607	0.543	0.474	0.398	0.318	0.236	0.199	0.161	0.124	0.089	0.055	0.025	0
$\frac{1}{4}$		0.869	0.790	0.708	0.623	0.533	0.438	0.338	0.294	0.247	0.200	0.151	0.102	0.052	0
$\frac{9}{4}$		1.019	0.925	0.830	0.733	0.632	0.526	0.414	0.364	0.310	0.255	0.198	0.136	0.072	0
$\frac{9}{4}$		1.059	0.961	0.862	0.762	0.657	0.547	0.430	0.379	0.323	0.266	0.206	0.142	0.075	0
$\frac{9}{4}$		1.084	0.984	0.883	0.780	0.673	0.561	0.441	0.388	0.332	0.273	0.211	0.146	0.078	0
$\frac{9}{4}$		1.179	1.070	0.960	0.848	0.732	0.610	0.480	0.423	0.361	0.298	0.234	0.160	0.084	0
8		1.634	1.481	1.330	1.179	1.022	0.859	0.683	0.606	0.522	0.434	0.340	0.238	0.127	0

The relationship between $\frac{S}{S_0}$ & f , and $\frac{S}{S_0}$ & z is illustrated in the following figs (11) and (12) respectively.

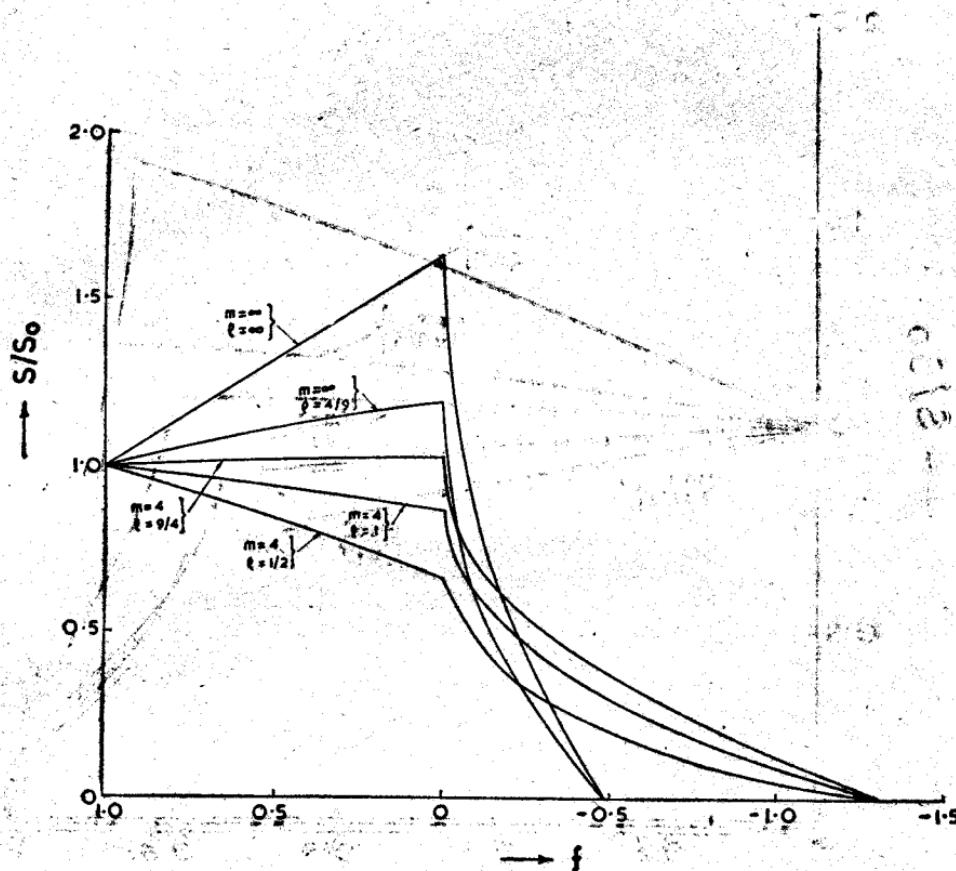


FIG. 11

Relation between $\frac{S}{S_0}$ & f for the tri-tubular charge
for some set of values of m & ρ

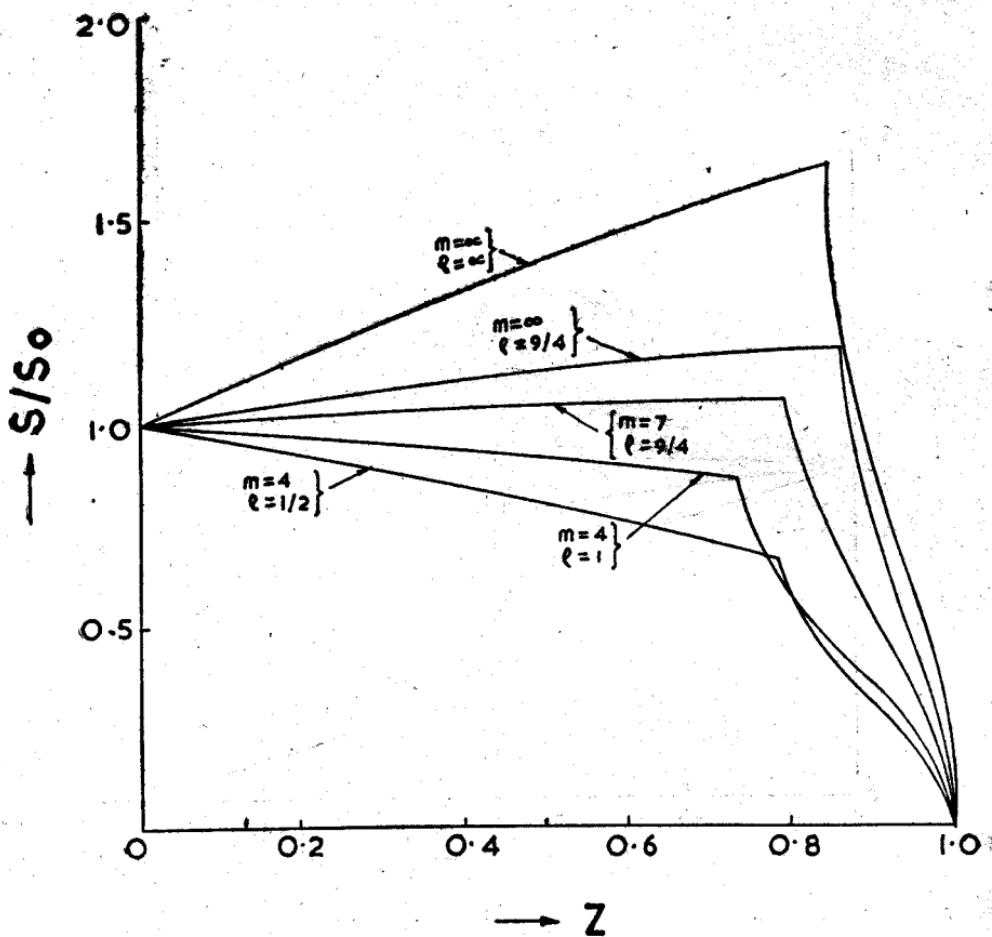


FIG 12

Relation between $\frac{S}{S_0}$ & ~~the~~ the tri-tubular charge
for some set of values of m, ℓ, p

(b) Quadra-tubular charge³:

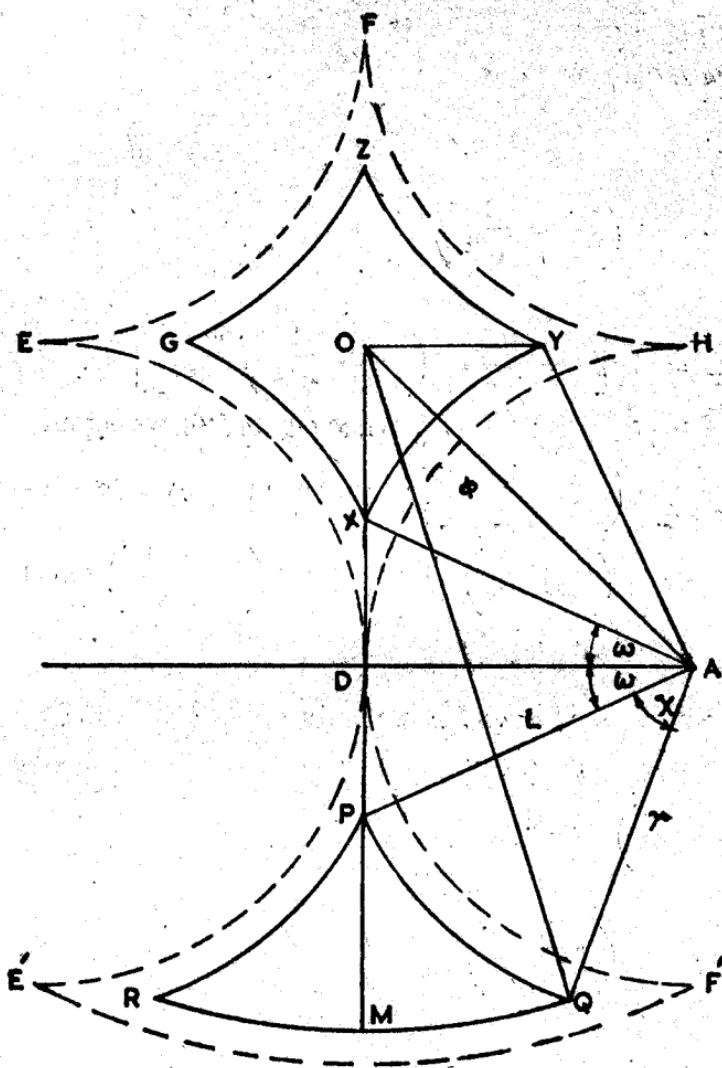


FIG. 13

length of the circumference of the $\triangle PQR$ is

$$= 2r\chi + a(2 + \sqrt{2} - \sec \omega)(90^\circ - 2\varphi) \\ = 2a[(2 + \sqrt{2})(45^\circ - \varphi) + (\varphi + \chi - 45^\circ) \sec \omega]. \quad (38)$$

and that of XYO is

$$= r(90^\circ - 2\omega) \\ = 2a(45^\circ - \omega) \sec \omega \quad \dots \quad \dots \quad \dots \quad \dots \quad \dots \quad (39)$$

In this case

$S =$ Four times (the length of the circumference of the $\triangle PQR +$ that of $XYO) \times$ height of the grain + eight times (the area of the $\triangle PQR +$ that of $XYO)$

$$= 8a L [(2 + \sqrt{2})(45^\circ - \varphi) + (\varphi + \chi - \omega) \sec \omega] + 8a^2 H(\omega) \quad 0^\circ \leq \omega \leq 45^\circ \quad (40)$$

Now

$$a = \frac{1}{2} \left(1 - \frac{1}{\sqrt{2}} \right) (m + 1) d \quad \dots \quad \dots \quad (41)$$

and

$$L = d \left[1 + \rho m - \left(1 - \frac{1}{\sqrt{2}} \right) \frac{m+1}{\cos \omega} \right] \quad \dots \quad \dots \quad (42)$$

Substituting for a and L from (41) and (42) in (40), we obtain

$$S = 4 \left(1 - \frac{1}{\sqrt{2}} \right) (m + 1) d^2 \left[\left\{ (2 + \sqrt{2})(45^\circ - \varphi) + (\varphi + \chi - \omega) \sec \omega \right\} \right. \\ \left. + \left\{ 1 + \rho m - \left(1 - \frac{1}{\sqrt{2}} \right) \frac{m+1}{\cos \omega} \right\} + \frac{1}{2} \left(1 - \frac{1}{\sqrt{2}} \right) (m + 1) H(\omega) \right] \quad \dots \quad \dots \quad (43)$$

Also

$$S_0 = \frac{1}{2} \pi d^2 (2m^2\rho + 8m\rho + m^2 - 4)$$

Dividing (43) by (44), the function of the progressivity of the powder is given by

$$\frac{S}{S_0} = \frac{8 \left(1 - \frac{1}{\sqrt{2}} \right) (m+1)}{\pi(2m^2\rho + 8m\rho + m^2 - 4)} \left[\left\{ (2 + \sqrt{2})(45^\circ - \varphi) + (\varphi + \chi - \omega) \sec \omega \right\} \right. \\ \left. + \left\{ 1 + \rho m - \left(1 - \frac{1}{\sqrt{2}} \right) \frac{m+1}{\cos \omega} \right\} + \frac{1}{2} \left(1 - \frac{1}{\sqrt{2}} \right) (m + 1) H(\omega) \right] \\ 0^\circ \leq \omega \leq 45^\circ \quad \dots \quad \dots \quad (45)$$

For $\omega = 0^\circ$, (45) gives

$$\frac{S}{S_0} = \frac{2 \left(1 - \frac{1}{\sqrt{2}} \right) (m+1)}{(2m^2\rho + 8m\rho + m^2 - 4)} \left[(5 + \sqrt{2}) \left\{ 1 + \rho m - \left(1 - \frac{1}{\sqrt{2}} \right) (m+1) \right\} \right. \\ \left. + \frac{1}{4}(5\sqrt{2} - 6)(m+1) \right]$$

which can be put in the form

$$\frac{S}{S_0} = \frac{m+1}{2(2m^2\rho + 8m\rho + m^2 - 4)} \left[2(8 - 3\sqrt{2})\rho m - (33m + 17) \right. \\ \left. + 2\sqrt{2}(11m + 8) \right]$$

This is the value of α at the end of the first period of burning.

The following table gives the values of $\frac{S}{S_0}$ as a function of ω for some set of values of m and ρ .

TABLE 2

m	ρ	ω												
		0°	5°	10°	15°	20°	25°	30°	32° 30'	35°	37° 30'	40°	42° 30'	45°
4	$\frac{1}{2}$	0.745	0.677	0.602	0.528	0.438	0.349	0.257	0.211	0.165	0.120	0.076	0.005	0
	1	0.926	0.838	0.748	0.654	0.557	0.456	0.349	0.294	0.237	0.179	0.119	0.060	0
4	$\frac{9}{4}$	1.053	0.952	0.850	0.748	0.642	0.534	0.414	0.352	0.288	0.221	0.150	0.078	0
	$\frac{9}{4}$	1.132	1.023	0.914	0.803	0.690	0.571	0.445	0.379	0.310	0.239	0.162	0.084	0
7	$\frac{9}{4}$	1.181	1.067	0.953	0.838	0.720	0.598	0.465	0.396	0.324	0.249	0.169	0.088	0
	$\frac{9}{4}$	1.366	1.234	1.103	0.970	0.833	0.690	0.539	0.459	0.376	0.289	0.196	0.102	0
8	∞	1.879	1.696	1.517	1.338	1.155	0.964	0.761	0.652	0.538	0.418	0.287	0.150	0

The relationship between S/S_0 & f , and S/S_0 & z is illustrated below in the figures (14) and (15) respectively.

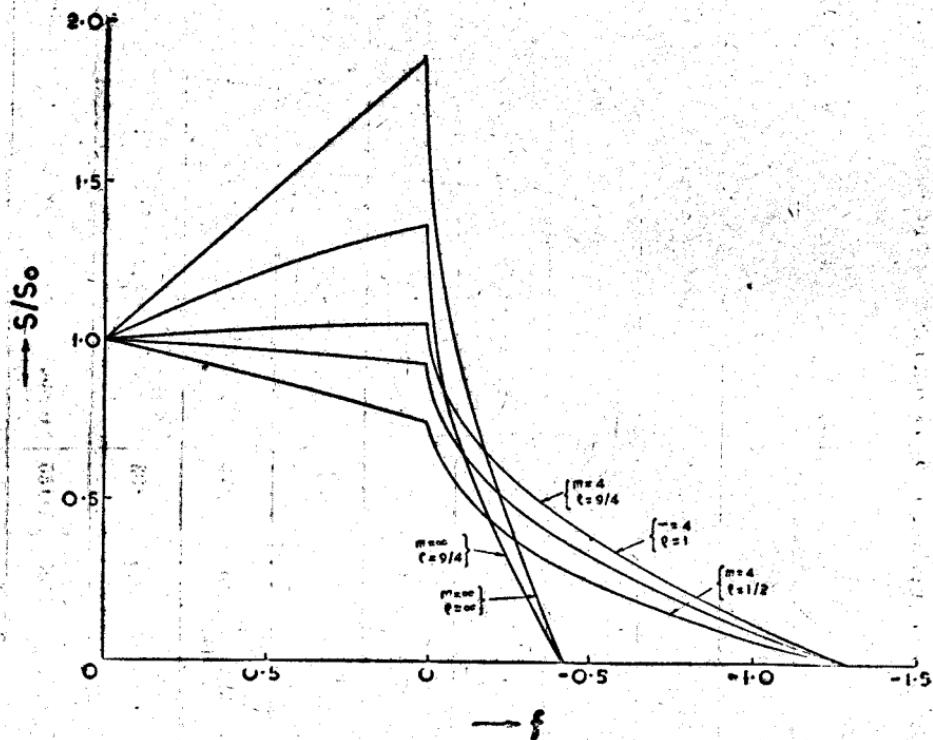


FIG 14

Relation between $\frac{S}{S_0}$ & f for the quadra-tubular charge
for some set of values of m & ρ

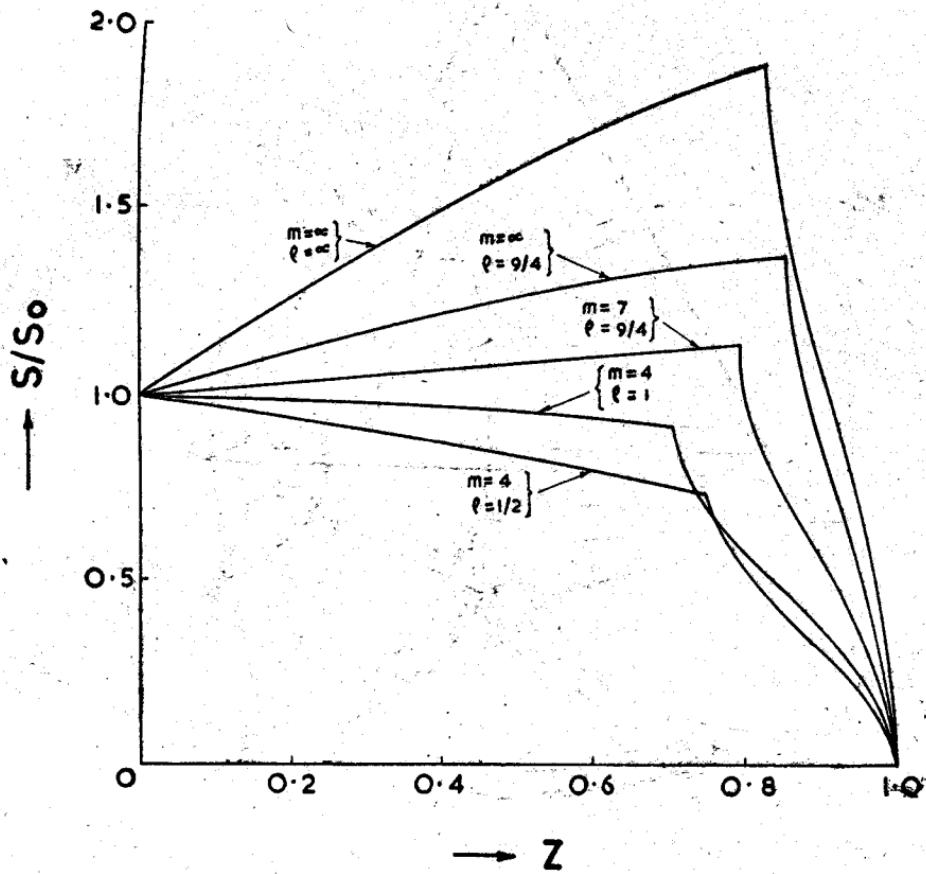


FIG 15

Relation between $\frac{S}{S_0}$ & z for the quadra-tubular charge
for some set of values of m & p .

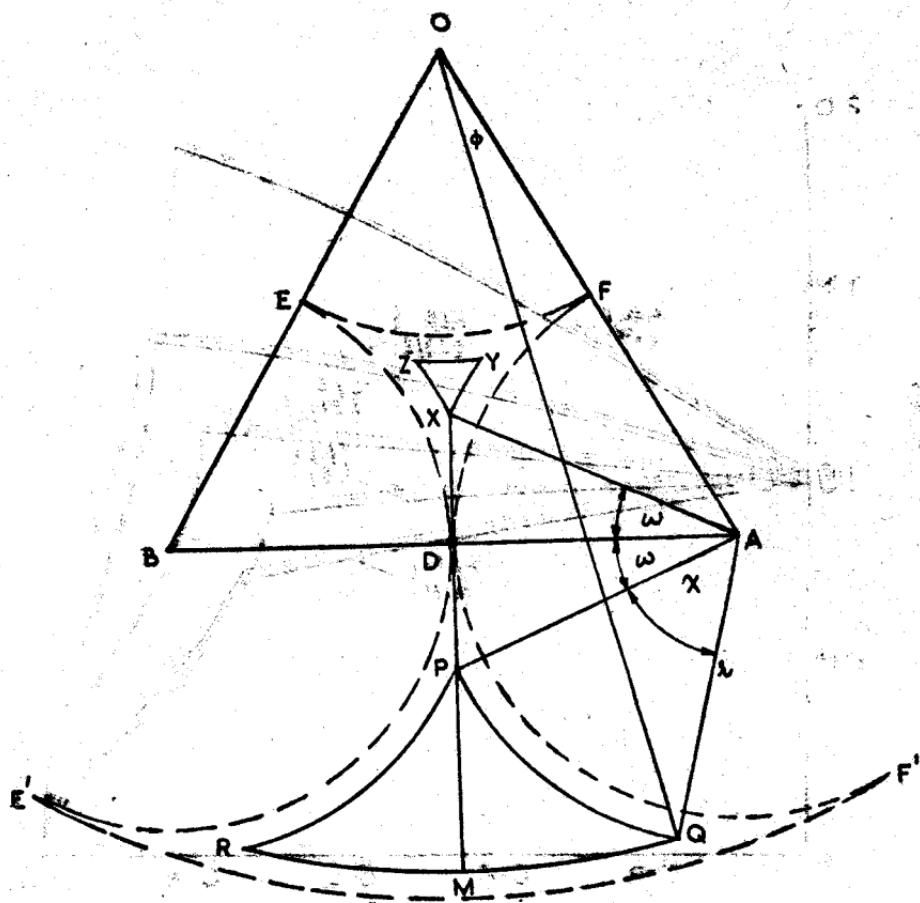
(c) Hepta-tubular charge⁴:

FIG. 16

Length of the circumference of the $\triangle PQR$ is

$$\begin{aligned}
 &= 2r\chi + (4a - r)(60^\circ - 2\varphi) \\
 &= 2a[4(30^\circ - \varphi) + (\varphi + \chi - 30^\circ) \sec \omega] \dots \dots \dots (46)
 \end{aligned}$$

and that of the $\triangle XYZ$ is

$$\begin{aligned}
 &= 3r(60^\circ - 2\omega) \\
 &= 6a(30^\circ - \omega) \sec \omega \dots \dots \dots \dots \dots (47)
 \end{aligned}$$

Now

$S =$ six times (the length of the circumference of the $\triangle PQR$ + that of the $\triangle XYZ$) \times height of the grain + twelve times (the area of the $\triangle PQR$ + that of the $\triangle XYZ$).

But the $\triangle XYZ$ disappears when $\omega = 30^\circ$.

\therefore For $0^\circ \leq \omega \leq 30^\circ$

$$S = 12aL \left\{ 4(36^\circ - \varphi) + (60^\circ + \varphi + \chi - 3\omega) \sec \omega \right\} + 12a^2 H(\omega) \quad (48a)$$

and for $30^\circ < \omega \leq 42^\circ 25'$

$$S = 12aL \left\{ 4(30^\circ - \varphi) + (\varphi + \chi - 30^\circ) \sec \omega \right\} + 12a^2 H(\omega) \quad (48b)$$

Now

$$a = \left(\frac{m+1}{8} \right) d \quad \dots \quad \dots \quad \dots \quad (49)$$

and

$$L = \left[1 + \rho m - \frac{m+1}{4 \cos \omega} \right] d \quad \dots \quad \dots \quad \dots \quad (50)$$

Substituting for a and L from (49) and (50) in (48), we obtain

$$S = \frac{3}{16}(m+1)d^2 \left[8 \left\{ 4(30^\circ - \varphi) + (60^\circ + \varphi + \chi - 3\omega) \sec \omega \right\} \right. \\ \left. \left(1 + \rho m - \frac{m+1}{4 \cos \omega} \right) + (m+1)H(\omega) \right] \quad 0^\circ \leq \omega \leq 30^\circ \quad (51a)$$

and

$$S = \frac{3}{16}(m+1)d^2 \left[8 \left\{ 4(30^\circ - \varphi) + (\varphi + \chi - 30^\circ) \sec \omega \right\} \right. \\ \left. \left(1 + \rho m - \frac{m+1}{4 \cos \omega} \right) + (m+1)H(\omega) \right] \quad 30^\circ \leq \omega \leq 42^\circ 25' \quad (51b)$$

Also

$$S_0 = \frac{1}{2}\pi d^2 (2m^2\rho + 14m\rho + m^2 - 7) \quad \dots \quad (52)$$

Dividing (51) by (52)

$$\frac{S}{S_0} = \frac{3(m+1)}{8\pi(2m^2\rho + 14m\rho + m^2 - 7)} \left[2 \left\{ 4(30^\circ - \varphi) + (60^\circ + \varphi + \chi - 3\omega) \right. \right. \\ \left. \left. \sec \omega \right\} \left(1 + \rho m - \frac{m+1}{4 \cos \omega} \right) + (m+1)H(\omega) \right] \quad 0^\circ \leq \omega \leq 30^\circ \\ \dots \quad \dots \quad \dots \quad (53a)$$

and

$$\frac{S}{S_0} = \frac{3(m+1)}{8\pi(2m^2\rho + 14m\rho + m^2 - 7)} \left[2 \left\{ 4(30^\circ - \varphi) + (\varphi + \chi - 30^\circ) \sec \omega \right\} \right. \\ \left. \left(1 + \rho m - \frac{m+1}{4 \cos \omega} \right) + (m+1)H(\omega) \right] \quad 30^\circ \leq \omega \leq 42^\circ 25' \\ \dots \quad \dots \quad \dots \quad (53b)$$

when $\omega = 0^\circ$, (53a) gives

$$\frac{S}{S_0} = \frac{(m+1)}{8(2m^2\rho + 14m\rho + m^2 - 7)} (40m\rho - 9m + 31)$$

This is the value of a at the end of the first period of burning.

In following table are shown the values of $\frac{S}{S_0}$, the values within the brackets correspond to those obtained by Tavernier¹.

TABLE 3

m	ρ	ω													
		0°	5°	10°	15°	20°	25°	30°	32°	30'	35°	37°	30'	40°	42°
4	0.884	0.779	0.669	0.555	0.438	0.317	0.194	0.154	0.114	0.075	0.036	0	0	(0.044)	(0)
	(0.884)	(0.737)	(0.645)	(0.546)	(0.441)	(0.331)	(0.211)	(0.172)	(0.131)	(0.088)	(0.044)	(0)	(0)		
4	0.999	0.878	0.756	0.632	0.504	0.371	0.233	0.188	0.142	0.096	0.048	0	0	(0.058)	(0)
	(0.999)	(0.829)	(0.728)	(0.621)	(0.507)	(0.389)	(0.254)	(0.211)	(0.164)	(0.113)	(0.068)	(0)	(0)		
4	1.072	0.941	0.811	0.680	0.546	0.406	0.258	0.210	0.160	0.109	0.055	0	0	(0.068)	(0)
	(1.072)	(0.888)	(0.781)	(0.668)	(0.550)	(0.425)	(0.282)	(0.236)	(0.185)	(0.129)	(0.068)	(0)	(0)		
7	1.238	1.087	0.937	0.786	0.631	0.469	0.298	0.243	0.186	0.126	0.064	0	0	(0.078)	(0)
	(1.238)	(1.026)	(0.902)	(0.772)	(0.635)	(0.492)	(0.326)	(0.273)	(0.214)	(0.149)	(0.078)	(0)	(0)		
10	1.348	1.184	1.020	0.856	0.687	0.511	0.324	0.265	0.202	0.138	0.069	0	0	(0.085)	(0)
	(1.348)	(1.116)	(0.982)	(0.840)	(0.692)	(0.536)	(0.355)	(0.297)	(0.234)	(0.163)	(0.085)	(0)	(0)		
8	1.841	1.617	1.394	1.169	0.938	0.698	0.444	0.362	0.277	0.188	0.095	0	0	(0.117)	(0)
	(1.841)	(1.525)	(1.341)	(1.148)	(0.945)	(0.732)	(0.485)	(0.406)	(0.320)	(0.223)	(0.117)	(0)	(0)		
8	2.5	2.194	1.893	1.591	1.283	0.960	0.615	0.504	0.388	0.266	0.135	0	0	(0.315)	(0)
	(2.5)	(2.067)	(1.820)	(1.562)	(1.293)	(1.007)	(0.673)	(0.567)	(0.449)	(0.315)	(0.167)	(0)	(0)		

The relationship between $\frac{S}{S_0}$ & f , and $\frac{S}{S_0}$ & z is illustrated in the following figures (17) and (18) respectively.

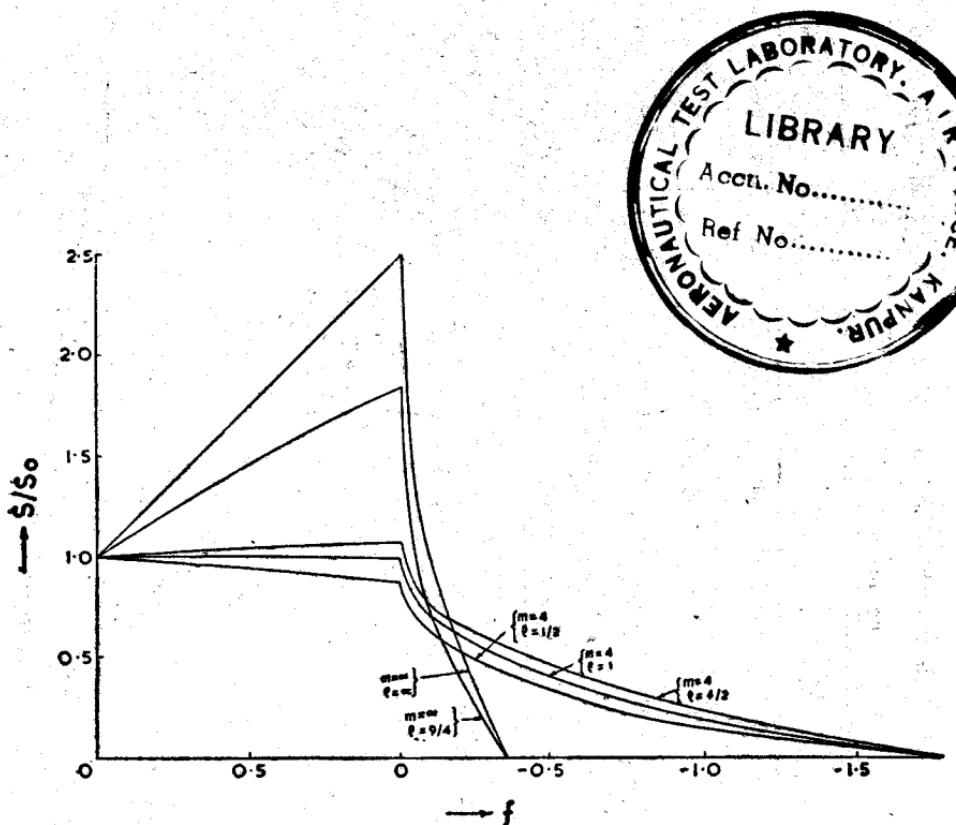


FIG 17

Relation between $\frac{S}{S_0}$ & f for the hepta-tubular charge
for some set of values m & ρ

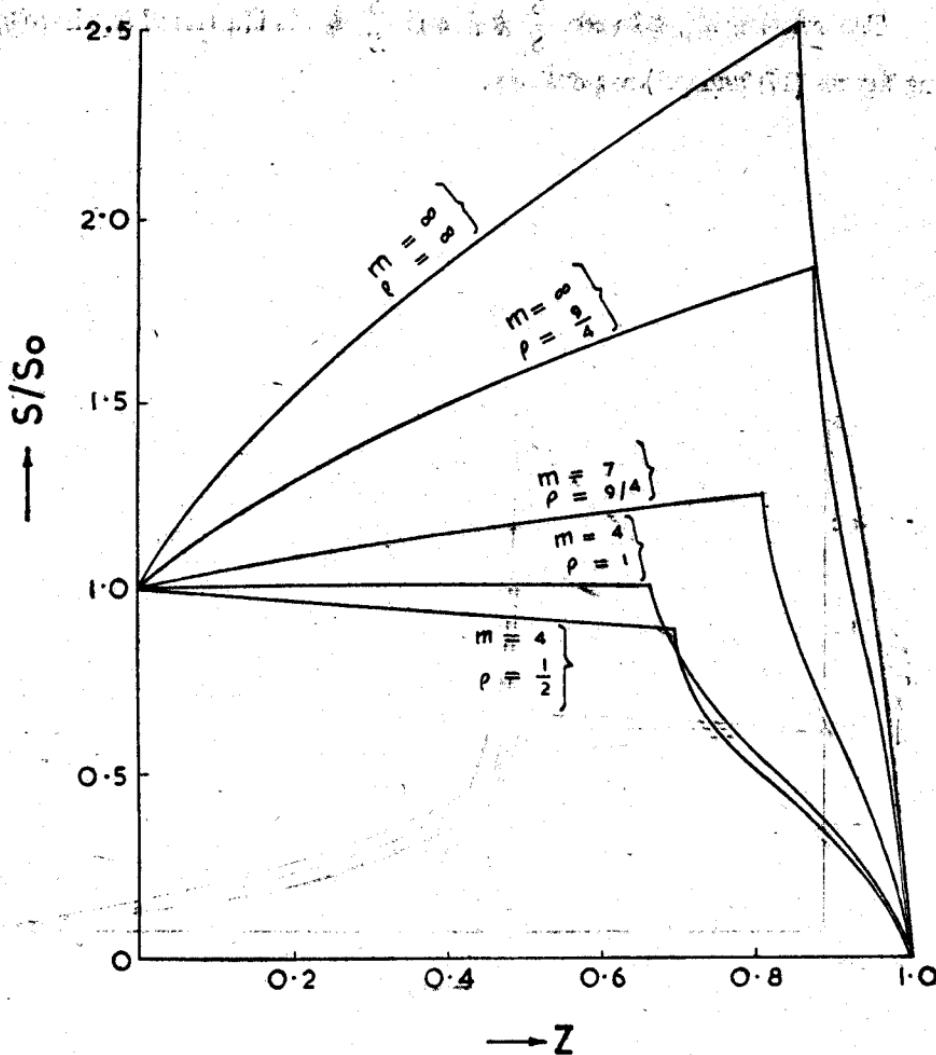


FIG 18

Relation between $\frac{S}{S_0}$ & z for the hepta-tubular charge

for some set of values of m & ρ

The expression for $\frac{S}{S_0}$ as obtained by Tavernier¹ is

$$\frac{S}{S_0} = \frac{-3(m+1)}{8\pi(2m^2\rho + 14m\rho + m^2 - 7)} \left[\left(4m\rho + 4 - \frac{m+1}{\cos \omega} \right) H'(\omega) \frac{\cos^2 \omega}{\sin \omega} - (m+1) H(\omega) \right] \quad \dots (54a)$$

$$= -\frac{3(m+1)}{8\pi(2m^2\rho + 14m\rho + m^2 - 7)} \left[4(\rho m + 1) K(\omega) - (m+1) I(\omega) \right] \quad \dots (54b)$$

where

$$I(\omega) = H'(\omega) \cot \omega + H(\omega) \dots \dots \dots \quad (55a)$$

and

$$K(\omega) = H'(\omega) \frac{\cos^2 \omega}{\sin \omega} \dots \dots \dots \quad (55b)$$

Comparing the above expression for $\frac{S}{S_0}$ with ours we see that

$$K(\omega) = -2 \left[4 \left(\frac{\pi}{6} - \phi \right) + \left(\frac{\pi}{3} + \phi + \chi - 3\omega \right) \sec \omega \right] \quad 0^\circ \leq \omega \leq 30^\circ \quad (56a)$$

$$= -2 \left[4 \left(\frac{\pi}{6} - \phi \right) + \left(\phi + \chi - \frac{\pi}{6} \right) \sec \omega \right] \quad 30^\circ \leq \omega \leq 42^\circ 25' \quad (56b)$$

We have calculated and collected the values of $K(\omega)$ in the following table, the values written within the brackets correspond to those obtained by Tavernier¹.

TABLE 4

ω	0°	5°	10°	15°	20°	25°
	-10.4720 (-10.4720)	-9.1884 (-8.6590)	-7.9280 (-7.6225)	-6.6648 (-6.5432)	-5.8738 (-5.4140)	-4.0224 (-4.2195)

ω	30°	$32^\circ 30'$	35°	$37^\circ 30'$	40°	$42^\circ 25'$
	-2.5744 (-2.8194)	-2.1122 (-2.3728)	-1.6260 (-1.8794)	-1.1142 (-1.3181)	-0.5672 (-0.6975)	0 (0)

Variation of $(S/S_0)_{max}$ for the tritubular charge²

It has been shown² that for a tritubular charge, $\frac{S}{S_0}$ is maximum for

$$f = \frac{(13m+9) - 3\sqrt{3}(m+1) - 4mp}{3[(3m-1) - \sqrt{3}(m+1)]} \dots \dots \dots \quad (57)$$

with

$$\rho_1 = \frac{m+3}{m} \quad \left. \begin{array}{l} \\ \end{array} \right\} \quad (58)$$

$$\rho_2 = \frac{(13m+9) - 3\sqrt{3}(m+1)}{4} \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

also

$$\left(\frac{S}{S_0}\right)_{max} = 1 \quad \text{for } \rho < \rho_1$$

$$= a + \frac{\beta^2}{4\gamma} \quad \rho_1 \leq \rho \leq \rho_2$$

$$= a \quad \rho > \rho_2$$

We shall now consider the following four cases :

Case I. Firstly we take $m=4$. Substituting for a , β and γ we obtain

$$\left(\frac{S}{S_0}\right)_{max} = \frac{8\rho(4\rho + 7) + 137}{3(56\rho + 13)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{7}{4} \text{ and } \rho_2 = \frac{61 - 15\sqrt{3}}{16}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 5

ρ	1.75 $(=\rho_1)$	2	2.189 $(=\rho_2)$	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.005	1.015	1.019	1.053	1.080	1.097	1.149	1.167

Case II. Secondly we take $m=7$. In this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{7\rho(7\rho + 10) + 169}{3(70\rho + 23)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{10}{7} \text{ and } \rho_2 = \frac{25 - 6\sqrt{3}}{7}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 6

ρ	1.429 $(=\rho_1)$	1.8	2.087 $(=\rho_2)$	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.015	1.042	1.059	1.115	1.159	1.187	1.276	1.307

Case III. Thirdly we take $m=10$. In this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{20\rho(10\rho + 13) + 629}{3(260\rho + 97)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{13}{10} \quad \text{and} \quad \rho_2 = \frac{139 - 33\sqrt{3}}{40}$$

We tabulate below the values of $\left(\frac{S}{S_o}\right)_{max}$ for some values of ρ .

TABLE 7

ρ	1.3 $(=\rho_1)$	2.046 $(=\rho_2)$	2.25	3	4	5	20	∞
$(S/S_o)_{max}$	1	1.058	1.084	1.151	1.204	1.237	1.344	1.383

Case IV. Fourthly we take $m=\infty$. In this case

$$\left(\frac{S}{S_o}\right)_{max} = \frac{2\rho(\rho+1)+5}{3(2\rho+1)} \quad \rho_1 \leqslant \rho \leqslant \rho_2$$

with

$$\rho_1 = 1 \quad \text{and} \quad \rho_2 = \frac{1}{2}(13 - 3\sqrt{3})$$

We tabulate below the values of $\left(\frac{S}{S_o}\right)_{max}$ for some values of ρ .

TABLE 8

ρ	1 $(=\rho_1)$	1.5	1.951 $(=\rho_2)$	2.25	3	4	5	20	∞
$(S/S_o)_{max}$	1	1.042	1.123	1.180	1.277	1.356	1.407	1.573	1.634

The results of the above four cases are illustrated below in Fig 19.

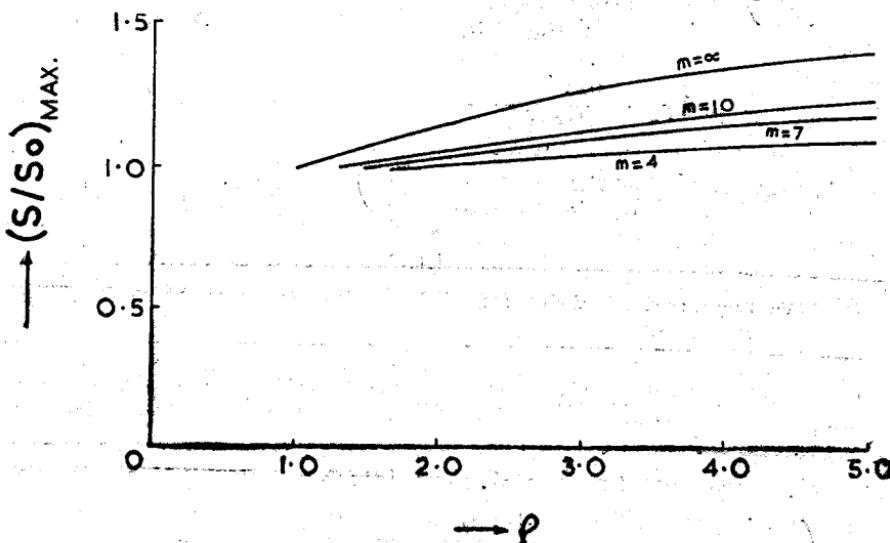


FIG 19

Variation of $\left(\frac{S}{S_o}\right)_{max}$ with ρ for the tri-tubular charges for some values of m

Variation of $\left(\frac{S}{S_0}\right)_{max}$ for the quadra-tubular charge

It has also been shown³ that for a quadra-tubular charge, $\frac{S}{S_0}$ is maximum for

$$f = \frac{(11m + 8)\sqrt{2} - 9(m + 1) - 3\sqrt{2}mp}{9[m\sqrt{2} - (m + 1)]} \quad \dots \quad (59)$$

with

$$\left. \begin{aligned} \rho_1 &= \frac{2}{3} \frac{m+4}{m} \\ \rho_2 &= \frac{(11m+8)\sqrt{2}-9(m+1)}{3\sqrt{2}m} \end{aligned} \right\} \quad \dots \quad (60)$$

Also

$$\begin{aligned} \left(\frac{S}{S_0}\right)_{max} &= 1 & \rho < \rho_1 \\ &= a + \frac{\beta^2}{4\gamma} & \rho_1 \leq \rho \leq \rho_2 \\ &= a & \rho > \rho_2 \end{aligned}$$

We shall now consider the following four cases:

Case I. Firstly we take $m=4$. Then substituting for a , β and γ we obtain

$$\left(\frac{S}{S_0}\right)_{max} = \frac{12\rho(3\rho + 4) + 91}{9(16\rho + 3)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{4}{3} \text{ and } \rho_2 = \frac{52\sqrt{2} - 45}{12\sqrt{2}}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 9

ρ	1.333 $(=\rho_1)$	1.682 $(=\rho_2)$	2	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.016	1.039	1.053	1.082	1.104	1.117	1.160	1.174

Case II. Secondly we take $m=7$. For this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{7}{9} \frac{3\rho(21\rho + 22) + 127}{(154\rho + 45)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{22}{21} \text{ and } \rho_2 = \frac{85\sqrt{2} - 72}{21\sqrt{2}}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 10

ρ	1.048 $(=\rho_1)$	1.623 $(=\rho_2)$	2	2.25	3		5	20	∞
$(S/S_0)_{max}$	1	1.055	1.106	1.132	1.185	1.227	1.254	1.337	1.366

Case III. Thirdly we take $m=10$. For this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{15\rho(15\rho + 14) + 412}{18(35\rho + 12)} \quad \rho_1 \leqslant \rho \leqslant \rho_2$$

with

$$\rho_1 = \frac{14}{15} \text{ and } \rho_2 = \frac{118\sqrt{2} - 99}{30\sqrt{2}}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 11

ρ	0.933 $(=\rho_1)$	1.6 $(=\rho_2)$	2	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.082	1.149	1.181	1.247	1.3	1.333	1.438	1.476

Case IV. Fourthly we take $m=\infty$. In this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{3\rho(3\rho + 2) + 13}{9(2\rho + 1)} \quad \rho_1 \leqslant \rho \leqslant \rho_2$$

with

$$\rho_1 = \frac{2}{3} \text{ and } \rho_2 = \frac{11\sqrt{2} - 9}{3\sqrt{2}}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 12

ρ	0.667 $(=\rho_1)$	1	1.545 $(=\rho_2)$	2	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.037	1.189	1.314	1.366	1.475	1.565	1.622	1.810	1.879

The results of the above four cases are illustrated below in Fig. 20.

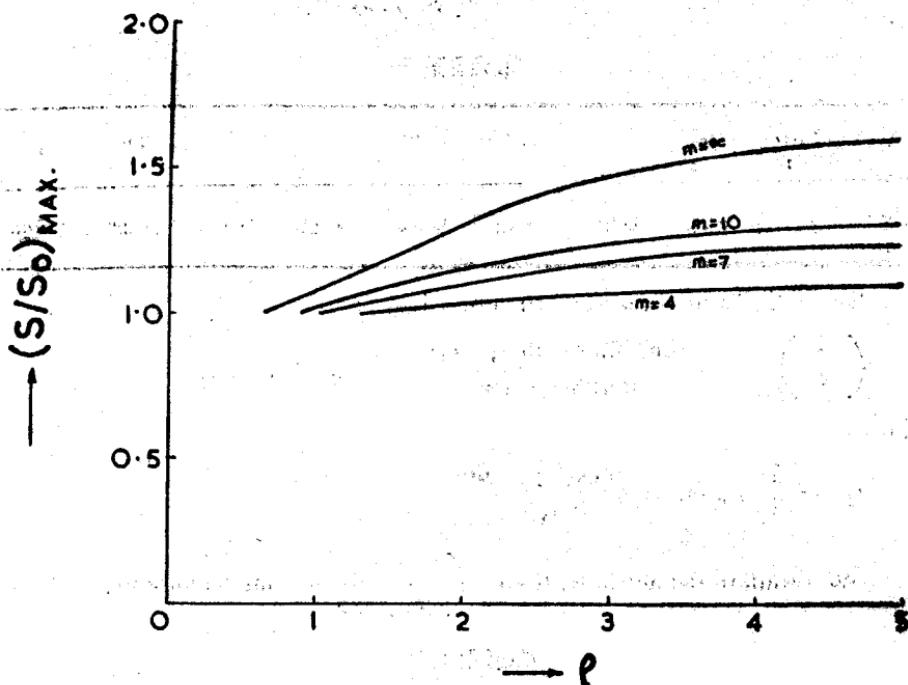


FIG 20

Variation of $\left(\frac{S}{S_0}\right)_{max}$ with ρ for quadra-tubular charge for some values of m

Variation of $\left(\frac{S}{S_0}\right)_{max}$ for the hepta-tubular charge

Tavernier¹ has shown that $\frac{S}{S_0}$ is maximum for

$$f = \frac{13m + 1 - 12m\rho}{9(m-3)} \quad \dots \quad \dots \quad \dots \quad (61)$$

with

$$\begin{aligned} \rho_1 &= \frac{m+7}{3m} \\ \rho_2 &= \frac{13m+1}{12m} \end{aligned} \quad \dots \quad \dots \quad \dots \quad (62)$$

Thus

$$\begin{aligned} \left(\frac{S}{S_0}\right)_{max} &= 1 & \rho < \rho_1 \\ &= a + \frac{\rho^2}{4\gamma} & \rho_1 \leq \rho \leq \rho_2 \\ &= a & \rho > \rho_2 \end{aligned}$$

We shall now consider the following four cases:

Case I. Firstly we take $m = 4$. Then substituting for α , β and γ , we obtain

$$\left(\frac{S}{S_0}\right)_{max} = \frac{24\rho(12\rho + 11) + 323}{9(88\rho + 9)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{11}{12} \text{ and } \rho_2 = \frac{53}{48}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 13

ρ	0.917 $(=\rho_1)$	1.104 $(=\rho_2)$	2	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.011	1.064	1.072	1.087	1.099	1.107	1.129	1.136

Case II. Secondly we take, $m = 7$. In this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{21\rho(3\rho + 2) + 55}{9(14\rho + 3)} \quad \rho_1 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{2}{3} \text{ and } \rho_2 = \frac{23}{21}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 14

ρ	0.667 $(=\rho_1)$	0.9	1.095 $(=\rho_2)$	1.5	2.25	3	4	5	20	∞
$(S/S_0)_{max}$	1	1.024	1.070	1.155	1.238	1.283	1.317	1.339	1.405	1.429

Case III. Thirdly we take $m=10$. In this case

$$\left(\frac{S}{S_0}\right)_{max} = \frac{60\rho(30\rho + 17) + 1415}{9(340\rho + 93)} \quad \rho_4 \leq \rho \leq \rho_2$$

with

$$\rho_1 = \frac{17}{30} \text{ and } \rho_2 = \frac{131}{120}$$

We tabulate below the values of $\left(\frac{S}{S_0}\right)_{max}$ for some values of ρ .

TABLE 15

ρ	0.567 ($=\rho_1$)	0.7	0.9	1.092 ($=\rho_2$)	1.5	2.25	3	4	5	20	∞
$(S/S_o)_{max}$	1	1.011	1.056	1.119	1.234	1.348	1.410	1.458	1.489	1.584	1.615

Case IV. Fourthly we take $m=\infty$. In this case

$$\left(\frac{S}{S_o}\right)_{max} = \frac{6\rho(3\rho+1)+11}{9(2\rho+1)} \quad \rho_1 \leqslant \rho \leqslant \rho_2,$$

with

$$\rho_1 = \frac{1}{3} \text{ and } \rho_2 = \frac{13}{12}$$

We tabulate below the values of $\left(\frac{S}{S_o}\right)_{max}$ for some values of ρ .

TABLE 16

ρ	0.338 ($=\rho_1$)	0.9	1.083 ($=\rho_2$)	2	2.25	3	4	5	20	∞
$(S/S_o)_{max}$	1	1.229	1.355	1.775	1.841	1.982	2.097	2.171	2.412	2.5

The results of the above four cases are illustrated in the following figure 21.

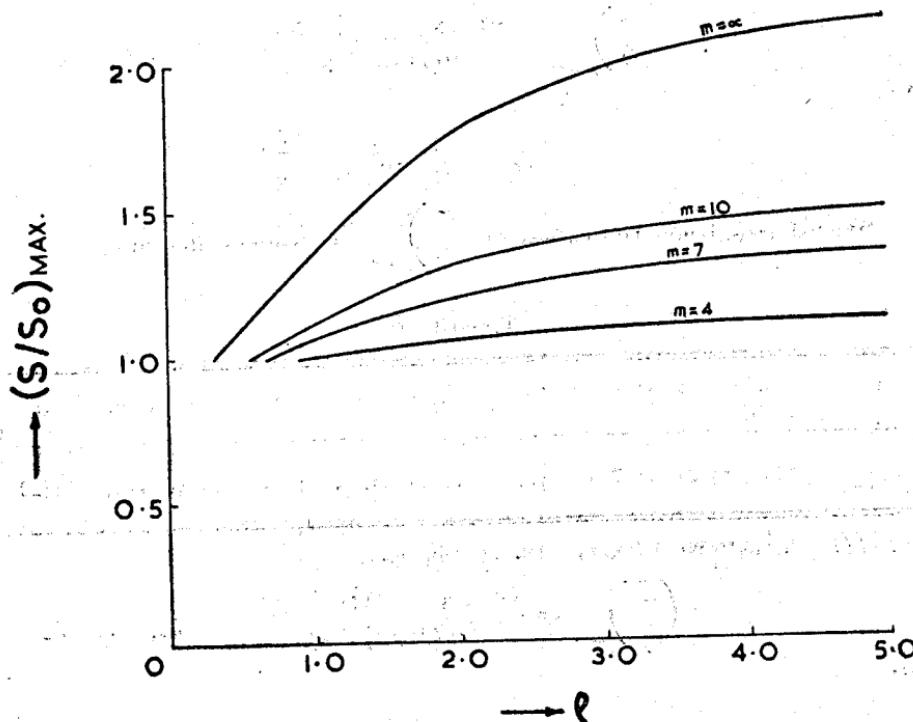


FIG 21

Variation $\left(\frac{S}{S_o}\right)_{max}$ with ρ for hepta-tubular charge for some values of m

We shall now examine the behaviour of $\left(\frac{S}{S_0}\right)_{max}$ when ρ is infinite, for the three charges. It is found that

$$\left(\frac{S}{S_0}\right)_{max} \text{ (for the tri-tubular charge)} = a = \frac{5 - \sqrt{3}}{2} \left(\frac{m+1}{m+3}\right)$$

$$\text{which is always } < \frac{5 - \sqrt{3}}{2}$$

$$\left(\frac{S}{S_0}\right)_{max} \text{ (for the quadra-tubular charge)}$$

$$= a = \frac{8 - 3\sqrt{2}}{2} \left(\frac{m+1}{m+4}\right)$$

$$\text{which is always } < \frac{8 - 3\sqrt{2}}{2}$$

$$\left(\frac{S}{S_0}\right)_{max} \text{ (for the hepta-tubular charge)}$$

$$= a = \frac{5}{2} \left(\frac{m+1}{m+7}\right)$$

$$\text{which is always } < \frac{5}{2}$$

In the following table are exhibited the values of $\left(\frac{S}{S_0}\right)_{max}$ for the three charges for some values of m .

TABLE 17

$(S/S_0)_{max}$	3	4	5	6	7	8	9	10	20	∞
m										
Tri-tubular ..	1.089	1.167	1.225	1.271	1.307	1.337	1.362	1.383	1.492	1.634
Quadra-tubular	1.073	1.174	1.252	1.315	1.366	1.409	1.445	1.476	1.644	1.879
Hepta-tubular	1	1.136	1.25	1.346	1.429	1.5	1.563	1.618	1.944	2.5

The above results are illustrated below in fig. 22.

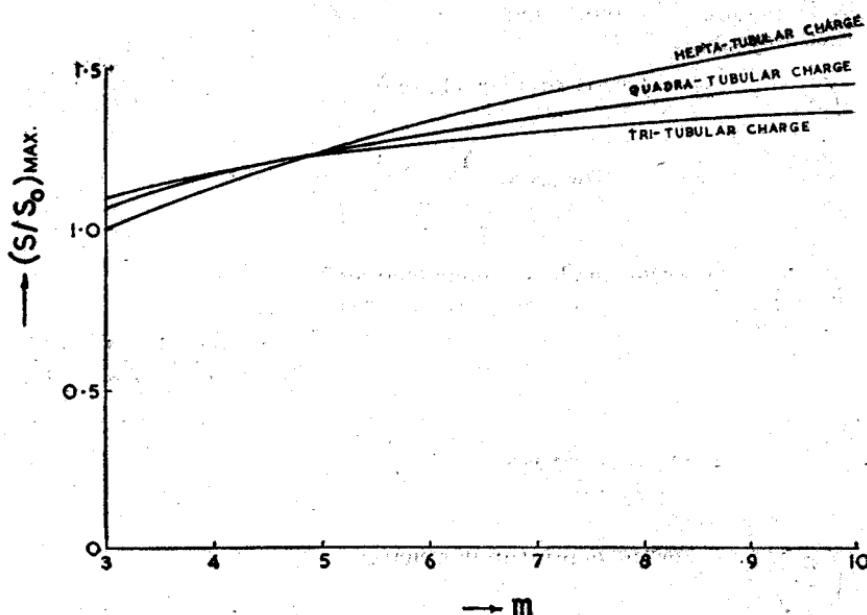


FIG 22

Variation of $(S/S_0)_{max}$ with m for the three charges
in the case when ρ is infinite

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