# LAMINAR SOURCE FLLOW OF SECOND ORDER FLUID BETWEEN TWO PARALLELL COAXIAL DISKS ROTATING AT DIFFERENT SPEEDS 

R. C. Chaudhary \& S. C. Rasvansut<br>M. R. Engineering College, Jaipur

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#### Abstract

The laminar source flow of second order fluid between two infinite parallel disks rotating with different velocities has been studied in this paper. The solution has been obtained by double series expansion about a known solution at a large radius. The effect of non-Newtonian parameters has been discussed on velocity profiles for small rotational Taylor numbers of the disks.


Laminar source flow between two parallel disks rotating at the same speed, has been investigated by Breitner \& Pohlhausen ${ }^{1}$ and Kreith \& Peube ${ }^{\text {² }}{ }^{3}$. Pelech \& Shapiro ${ }^{4}$ have obtained an approximate first order solution when one disk is rotating and the other is stationery as a byproduct of an investigation of the deflection of a rotating magnetic recording device. Kreith \& Viviand ${ }^{5}$ considered axisymmetric flow between two disks, rotating at different angular velocities with a source at the centre. The Reynolds number $R e$ based on source strength and the Taylor numbers $\alpha_{i}(i=1,2)$ associated with angular velocity of each disk, are all assumed to be small. The problem is solved by expanding the flow variables in powers of $R e$ about a known solution. This solution is also represented in a series expansion with $\alpha_{i}$ as perturbation parameter. The results are valid for small values of $\alpha_{i}$ and at a distance $r \gg R e^{1 / 2} / \alpha_{i}$. Recently it has been shown by Mellor ${ }^{6}$ et al., that the steady flow of a viscous ineompressible fluid between two coaxial infinite disks, one rotating and the other at rest with zero source flow, does not give a unique solution.

The source flow of an incompressible second order fluid between two parallel disks, one rotating and the other at rest, has been investigated by Rajvanshi?. The constitutive equations of an incompressible second order fluid as suggested by Coleman \& Noll8 are :

$$
\begin{gather*}
\tau_{i j}=-p g_{i j}+\phi_{1} A_{i j}+\phi_{2} B_{i j}+\phi_{3} A_{i k} A_{k j},  \tag{1}\\
A_{i j}=v_{i, j}+v_{j, i} \tag{2}
\end{gather*}
$$

and

$$
\begin{equation*}
B_{i j}=a_{i, j}+a_{j, i}+2 v_{m i} v_{m, j} . \tag{3}
\end{equation*}
$$

Where $\tau_{i j}$ is the stress tensor ; $g_{i j}$, the metric tensor ; $v_{i}$, the velocity vector; $a_{i}$, the acceleration vector ; $p$, the pressure; $\phi_{1}, \phi_{2}, \phi_{3}$, the fluid parameters and comma(,) denotes covariant differentiation. Rajvanshi ${ }^{7}$ obtained the solution by expanding flow variables in powers of the radius vector. The functions in the series expansion have been determined for small Reynold number depending on the angular velocity of rotation of the disk.

In the present paper the source flow of the second order fluid, between two parallel coaxial disks rotating at different speeds, defined by (1), (2), and (3), has been investigated. The series expansion method of Kreith \& Viviand ${ }^{5}$ has been adopted in this paper to obtain the solution. We note that the solution for zero source strength is not affected by the non-Newtonian parameters upto second order terms in Taylor number. But the effect of non-Newtonian parameters is present in the higher order approximations. In particular, it has been observed that the non-Newtonian parameters are most effective in perturbation terms of radial velocity when the two disks rotate in opposite direction, and the least, when the disks rotate in same direction with equal velocity.
EQUATIONS OF MOTION

The momentum equation for the incompressible flow is

$$
\begin{equation*}
\rho v_{j} v_{i, j}=\tau_{i j j j}, \tag{4}
\end{equation*}
$$

and the equation of continuity is

$$
\begin{equation*}
v_{i, i}=0 . \tag{5}
\end{equation*}
$$

We shall use polar cylindrical coordinates $(\bar{r}, \bar{\theta}, \bar{z})$ in the following discussion. The flow takes place between two parallel disks $z=+a$ and $z=-a$. Let the upper and lower disks rotate at angular velocities $\omega_{2}$ and $\omega_{1}$ respectively. The volumetric flow rate of the source (Strength) is to be assumed as $Q$.

Therefore the boundary conditions become

$$
\left.\begin{array}{ll}
\bar{u}=\bar{w}=0 & \text { at } \quad \bar{z}= \pm a,  \tag{6}\\
\bar{v}=\bar{r} \omega_{1} & \text { at } \quad \bar{z}=-a, \\
\bar{v}=\bar{r} \omega_{2} & \text { at } \quad \bar{z}=+a ; \\
\int_{-a}^{+a} 2 \pi \bar{r} \bar{u} d \bar{z}=Q .
\end{array}\right\}
$$

Let us introduce the following non-dimensional quantities-

$$
\left.\begin{array}{l}
r=\bar{r} / a, \bar{z}=\bar{z} / a, \\
u=\frac{\rho \bar{u} a}{\phi_{1}}, v=\frac{\rho \bar{v} a}{\phi_{1}}, w=\frac{\rho \bar{w} a}{\phi_{1}},  \tag{7}\\
p=\frac{\rho \bar{p} a^{2}}{\phi_{1}^{2}}, K=\frac{\phi_{2}}{\rho a^{2}}, S=\frac{\phi_{3}}{\rho a^{2}},
\end{array}\right\}
$$

Equations (6) and (7) now give the boundary conditions in the following form

$$
\left.\begin{array}{ll}
u=w=0 & \text { at } z= \pm 1,  \tag{8}\\
\int_{-1}^{+1} u d z & =\frac{2 R e}{r}, \\
v=\alpha_{1} r & \text { at } z=-1, \\
v=\alpha_{i} r & \text { at } z=+1 .
\end{array}\right\}
$$

where

$$
R e \text { (Reynolds number) }=\frac{Q \rho}{4 \pi a \phi_{1}}
$$

$\alpha_{1}$ (Taylor number for lower disk) $=\frac{\omega_{1} a^{2} \rho}{\phi_{3}}$.
$\alpha_{2}$ (Taylor number for upper disk) $=\frac{\omega_{2} a^{2} \rho}{\phi_{1}}$.
Let us define a stream function $\psi$ as

$$
\begin{equation*}
u=\frac{1}{r} \frac{\partial \psi}{\partial z}, w=-\frac{1}{r} \frac{\partial \psi}{\partial r} \tag{9}
\end{equation*}
$$

Following Kreith \& Viviand ${ }^{5}$, the solution, which is valid for large values of $r / R e^{1 / 2}$, is assumed in the following form :

$$
\begin{gather*}
\psi=r^{2} f_{-1}(z)+\operatorname{Re}\left\{f_{1}(z)+\frac{R e}{r^{2}} f_{3}(z)+\cdots\right\},  \tag{10}\\
p=r^{2} h_{-2}(z)+h_{0}(z)+\operatorname{Re}\left\{h(z) \ln r+\frac{R e}{r^{2}} h_{2}(z)+\cdots\right\}, \tag{11}
\end{gather*}
$$

and.

$$
\begin{equation*}
v=r g_{-1}(z)+R e^{1 / 2}\left\{\frac{R e^{1 / 2}}{r} g_{1}(z)+\frac{R e^{3 / 2}}{r^{3}} g_{3}(z)+\ldots\right\} \tag{12}
\end{equation*}
$$

Let us convert (1) to (5) into cylindrical polar coordinate system, and non-dimensionalise them by using (7). Substituting (9) to (12) in these non-dimensionalised equations and equating the coefficients of like powers of $r$, we obtain an infinite set of simultaneous ordinary differential equations. The first two systems are :

## System I

$$
\begin{align*}
& f^{\prime \prime \prime}-1+2 f_{-1} f_{-1}^{\prime \prime}-f^{\prime 2}-1=2 h_{-2}-g_{-1}^{2}+K\left[f_{-1} f^{i v}-2 f_{-1}^{\prime \prime 2}\right]+ \\
& +S\left[g_{-1}^{\prime 2}-2 f^{\prime \prime 2}{ }_{-1}+2 f_{-1}^{\prime} f_{-1}^{\prime \prime \prime}\right]  \tag{13}\\
& g_{-1}^{\prime \prime}+2 f_{-1} g_{-1}^{\prime}-2 g_{-1} f_{-1}^{\prime}=K\left[2 f_{-1} g^{\prime \prime \prime}-1-2 f_{-1}^{\prime \prime} g_{-1}^{\prime}\right]+ \\
& +S\left[2 f_{-1}^{\prime} g_{-1}^{\prime \prime}-2 f_{-1}^{\prime \prime} g_{-1}^{\prime}\right]  \tag{14}\\
& h_{-2}^{\prime}=2(2 K+S)\left[f^{\prime \prime \prime}{ }_{-1} f_{-1}^{\prime \prime}+g_{-1}^{\prime \prime} g_{-1}^{\prime}\right] . \tag{15}
\end{align*}
$$

The differential equation for $h_{0}$ is

$$
\begin{align*}
h_{0}^{\prime}= & -4 f^{\prime}{ }_{-1} f_{-1}-2 f^{\prime \prime}-1_{1}+4 K\left[f^{\prime \prime \prime}{ }_{-1} f_{-1}+11 f^{\prime \prime}{ }_{-1} f^{\prime}{ }_{-1}+\operatorname{Re}\left(f^{\prime \prime \prime}-1_{1} f_{1}^{\prime \prime}+\right.\right. \\
& \left.\left.+g_{1}^{\prime} g^{\prime \prime}-1+g_{1}^{\prime \prime} g_{-1}^{\prime}+f_{-1}^{\prime \prime} f_{1}^{\prime \prime \prime}\right)\right]+2 S\left[14 f_{1}^{\prime \prime} f_{-1}^{\prime} f_{-1}+\operatorname{Re}\left(g_{1}^{\prime \prime} g_{-1}^{\prime}+\right.\right. \\
& \left.\left.+g_{1}^{\prime} g_{-1}^{\prime \prime}+f^{\prime \prime \prime}{ }_{-1} f_{1}^{\prime \prime}+f^{\prime \prime}{ }_{-1} f_{1}^{\prime \prime \prime}\right)\right] . \tag{16}
\end{align*}
$$

System II

$$
\begin{align*}
& f^{\prime \prime \prime}{ }_{1}+2 f_{-1} f_{1}^{\prime \prime}=h-2 g_{-1} g_{1}+2 K\left[f_{-1}^{\prime} f^{\prime \prime \prime}+f_{-1} f_{1}{ }^{i \theta}+2 g_{-1}^{\prime \prime} g_{1}+2 g_{1}^{\prime} g_{-1}^{\prime}+\right. \\
& \left.+f_{1}^{\prime \prime} f^{\prime \prime}{ }_{-1}+f_{1}^{\prime} f^{\prime \prime \prime}{ }_{-1}\right]+2 S\left[f_{1-1}^{\prime} f^{\prime \prime \prime}{ }_{-1}+g_{1} g_{-1}^{\prime \prime}+f_{-1}^{\prime \prime} f_{1}^{\prime \prime}+\right. \\
& \left.+f_{-1}^{\prime} f_{1}^{\prime \prime}{ }_{1}+2 g_{-1}^{\prime} g_{1}^{\prime}\right],  \tag{17}\\
& g_{1}^{\prime \prime}+2 g_{1}^{\prime} f_{-1}=2 g_{-1} f_{1}^{\prime}+2 K\left[-2 f_{1}^{\prime} g_{-1}^{\prime}+g_{1}^{\prime \prime \prime} f_{-1}+g_{1}^{\prime \prime} f_{-1}^{\prime}+g_{1}^{\prime} f_{-1}^{\prime \prime}+\right. \\
& \left.+g_{1} f^{\prime \prime \prime}{ }_{-1}-2 f_{1}^{\prime \prime} g_{-1}^{\prime}\right]+2 S\left[g_{1} f_{-1}^{\prime \prime \prime}-2 f_{1}^{\prime} g_{-1}^{\prime}-f_{1}^{\prime} g_{-1}^{\prime \prime}+\right. \\
& \left.+f^{\prime}{ }_{-1} g_{1}^{\prime \prime}+g_{1}^{\prime} f^{\prime \prime}{ }_{-1}\right] \text {, }  \tag{18}\\
& h^{\prime}=0 . \tag{19}
\end{align*}
$$

and
The boundary conditions in the modified form are:

$$
\left.\begin{array}{c}
f_{n}^{\prime}( \pm 1)=0, \quad \text { for } n=-1,1,3 \ldots, \\
f_{n}( \pm 1)=0, \quad \text { for } n=-1,3, \ldots, \\
f_{1}(1)-f_{1}(-1)=2 . \\
f_{1}(-1)=0, \\
f_{1}(1)=2  \tag{23}\\
g_{s}( \pm 1)=0, \text { for } s=1,3, \ldots \\
g_{-1}(-1)=\alpha_{1}, \text { and } \\
g_{-1}(+1)=\alpha_{2} .
\end{array}\right\}
$$

We choose

In the above equations the prime denotes the differential coefficient with respect to $z$. The equation of continuity is identically satisfied by (9).

## System 1

We take Taylor series expansion for $f_{-1}, g_{-1}$ and $h_{-2}$ in the following form :

$$
\left.\begin{array}{l}
f_{-1}=\alpha_{1}^{2} F_{11}+2 \alpha_{1} \alpha_{2} F_{12}+\alpha_{2}^{2} F_{22}+\cdots  \tag{24}\\
g_{-1}=\alpha_{2} G_{1}+\alpha_{2} G_{2}+\alpha_{1}^{2} G_{11}+2 \alpha_{1} \alpha_{2} G_{12}+\alpha_{2}^{2} G_{22}+\cdots \\
h_{-2}=\alpha_{1}^{2} H_{11}+2 \alpha_{1} \alpha_{2} H_{12}+\alpha_{2}^{2} H_{22}+\cdots
\end{array}\right\}
$$

We substitute (24) in the equations of system I. On equating equal powers of $\alpha_{1}, \alpha_{2}$, and their products, we obtain four sub-systems of differential equations. These are readily solvable and the solutions are:

$$
\begin{align*}
& f_{-1}=-\frac{1}{240}\left(z^{2}-1\right)^{2}\left[\alpha_{1}^{2}(z-1)-2 \alpha_{1} \alpha_{2} z+\alpha_{2}^{2}(z+5)\right]+O\left(\alpha^{4}\right),  \tag{25}\\
& g_{-1}=-\frac{1}{2} \alpha_{1}(z-1)+\frac{1}{2} \alpha_{2}(z+1)+O\left(\alpha^{3}\right)  \tag{26}\\
& h_{-2}=\frac{3}{20}\left(\alpha_{1}^{2}+\alpha_{2}^{2}\right)+\frac{1}{5} \alpha_{1} \alpha_{2}+O\left(\alpha^{4}\right) \tag{27}
\end{align*}
$$

where $O\left(\alpha^{n}\right)$ meaus terms of $O\left(\alpha_{1}^{n}\right)$ or $\left(\alpha_{2}^{n}\right)$. We have also from (20)

$$
\begin{equation*}
f_{-1}^{\prime}=-\frac{1}{240}\left(z^{2}-1\right)\left[5\left(z^{2}-1\right)\left(\alpha_{2}-\alpha_{1}\right)^{2}+20\left(\alpha_{2}^{2}-\alpha_{1}^{2}\right) z\right]+O\left(\alpha^{4}\right), \tag{28}
\end{equation*}
$$

which agrees with Kreith \& Viviand ${ }^{5}$. Hence for zero source strength, the flow pattern remains unaffected by non-Newtonian fluid parameters ipto second order terms in the Taylor number $\alpha_{i}(i=1,2)$. It is sufficient to consider the value of $\alpha\left(=\alpha_{1} / \alpha_{2}\right)$ between -1 and +1 , since changing $\alpha$ into $1 / \alpha$ gives the flow field upside down. These results are valid for small values of $\alpha_{1}$ and $\alpha_{2}$.

Equation (25) shows that $w$ is always positive if $-2 / 3<\alpha<1$, but changes sign once if $-1 \leqslant \alpha<-2 / 3$, at a value of $z$ equal to $z^{*}=5 \frac{\alpha+1}{\alpha-1}$. Kreith \& Viviand ${ }^{5}$, have shown that the plane $z=z^{*}$ is a stream surface which divides the flow field into two separate regions. The dividing stream surface, when it exists, rotate with the dimensionless angular velocity $\alpha^{*}=-2 \alpha_{2}(\alpha+1)$ in the direction as the lower disk rotates. Since $u$ is not zero at $z=z^{*}$, the dividing $\mathrm{g}^{\text {lane }}$ is not analogous to a solid disk. When $\alpha$ increases from -1 to $(-2 / 3),\left(\alpha^{*} / \alpha_{1}\right)$ increases from 0 to +1 , whereas $\left(\alpha^{*} / \alpha_{2}\right)$ decreases from 0 to $(-2 / 3)$. Casal ${ }^{9}$ pointed out that for $\alpha_{i}=0$, the series solution converges when $\left|\alpha_{2}\right|<0 \cdot 17$.

## System II

We assume the Taylor series expansion for $f_{1}, g_{1}$ and $h$ in the form

$$
\begin{equation*}
x=\chi_{0}+\alpha_{1} \chi_{1}+\alpha_{2} \chi_{2}+\alpha_{1}^{2} x_{11}+2 \alpha_{1} \alpha_{2} \chi_{12}+\alpha_{2}^{2} \chi_{22}+\ldots \tag{29}
\end{equation*}
$$

As the system possesses non-zero solution for $\alpha_{1}=\alpha_{2}=0$, the zero order terms in (29) have been included.

By substituting (24) and (29) in system II [i.e. equations (17) to (19)], and equating like powers of Taylor numbers, we obtain a set of ordinary linear differential equations connecting the functions assumed in (29). These equations haverbeen solved ưsing modified boundary conditions. The solution in the final form is :

$$
\begin{aligned}
f_{1}= & \frac{1}{2}\left[2+3 z-z^{3}\right]+\frac{1}{1120}\left(\alpha_{1}^{2}+\alpha_{2}^{2}\right)\left[\frac{1}{9} z^{9}-\frac{2}{5} z^{7}-\frac{56}{5} z^{5}+\frac{1042}{45} z^{3}\right. \\
& \left.-\frac{35}{3} z\right]+\frac{1}{1120}\left(\alpha_{1}^{2}-\alpha_{2}^{2}\right)\left[-\frac{1}{4} z^{8}+7 z^{6}-\frac{63}{2} z^{4}+43 z^{2}-\right.
\end{aligned}
$$

$$
\begin{align*}
& \left.\quad-\frac{73}{4}\right]+\frac{1}{280} \alpha_{1} \alpha_{2}\left[-\frac{1}{18} z^{9}+\frac{13}{15} z^{7}-\frac{42}{5} z^{5}+\frac{649}{45} z^{3}-\frac{41}{6} z\right]+ \\
& \\
& +\frac{1}{80}(K+S)\left(\alpha_{1}^{2}+\alpha_{2}{ }^{2}\right)\left[-\frac{1}{7} z^{7}+\frac{23}{15} z^{5}-\frac{277}{105} z^{3}+\frac{131}{105} z\right]+ \\
& \\
& +\frac{1}{80}(K+S)\left(\alpha_{1}^{2}-\alpha_{2}^{2}\right)\left[-z^{6}-5 z^{4}+13 z^{2}-7\right]+\frac{1}{4200}(K+S)  \tag{30}\\
& \\
& \quad \alpha_{1} \alpha_{2}\left[-24 z^{7}-\frac{49}{2} z^{5}+121 z^{3}-\frac{145}{2} z\right]+\frac{1}{10}(K+S)^{2}\left(\alpha_{1}-\alpha_{2}\right)^{2}  \tag{31}\\
& \\
& \\
& \quad\left[\quad\left[z^{5}-2 z^{3}+z\right],\right. \\
& y_{1}=\frac{1}{40}\left(1-z^{2}\right)\left[5\left(\alpha_{1}+\alpha_{2}\right)\left(z^{2}-5\right)+z\left(\alpha_{2}-\alpha_{1}\right)\left(3 z^{2}-7\right)\right]+ \\
& \quad+(K+S)\left(\alpha_{1}-\alpha_{2}\right)\left(z-z^{3}\right)
\end{align*}
$$


and

$$
\begin{align*}
& h=-3-\frac{1}{525}\left[263\left(\alpha_{1}^{2}+\alpha_{2}^{2}\right)+494 \alpha_{1} \alpha_{2}-3\right. \\
& \left.\cdot(K+S)\left\{4\left(\alpha_{1}^{2}+\alpha_{2}^{2}\right)+31 \alpha_{1} \alpha_{2}\right\}\right]+\frac{4}{5} \\
& \cdot(K+S)\left(\alpha_{1}-\alpha_{2}\right)^{2} \tag{32}
\end{align*}
$$

If we put $K=S=0$ in (30) to (32), these agree with the corresponding equations of Kreith \& Viviand ${ }^{5}$. The effect of non-Newtonian parameters has been shown graphically on the perturbation term of order $\alpha_{2}{ }^{2}$ in $f_{1}^{\prime}$. In Fig. 1, $\left[\left(f_{1}^{\prime}-P_{0}^{\prime}\right) / \alpha_{2}{ }^{2}\right] \times 10^{2}$ has been plotted against $z$ for $\alpha=1$ i.e. both the disks ratate in the same direction with same angular velocity. The curves have been drawn for $K=S=0$ (Newtonian case) and $K=$ $-0: 1, S=0.35$. We note that the profiles are symmetrical about $z=0$. The effect of non-Newtonian parameter on $\left[\left(f_{1}^{\prime}-p_{0}^{\prime}\right) / \alpha_{2}^{2}\right] \times 10^{2}$ is very small. Fig. 2 gives the profiles for (i) $K=S=0$, (ii) $K=-0 \cdot 1$, $S=0.25$ and (iii) $K=-0 \cdot 1, S=0.35$ at $\alpha=0$, i.e. when the lower disk is stationary and upper sotates with given angular velocity. Inthis case, we note that the profile is not symmetrical about $z=0$. The effect of non-Newtonian parameters is more marked in comparison to the case $\alpha=1$. In Fig. 3, the profiles have been drawn for (i) $K=S=0$, (ii) $K=-0 \cdot 1, S=0 \cdot 25$, and (iii) $K=-0.1, S=0.35$ at $\alpha=-1$, i.e. the $t_{\text {wo }}$ disks rotate in opposite directions with equal angular velocities. The profiles are symmetrical about $z=0$. The effect of non-Newtonian parameters is more marked in comparison to $\alpha=0$ and 1 . We infer that the effect of non-Newtonian parameters is most conspicuous when torsion of the fluid takes place.

Fig. 1-Variation of $\left[\left(f_{1}^{\prime}-P o^{\prime}\right) / \alpha_{q}^{2}\right] \times 10^{2}$ with z for $a=1$,


Fig. 2-Variation of $\left[\left(f_{1}^{\prime}-P o^{\prime}\right) / \alpha_{2}{ }^{2}\right] \times 10^{2}$ with z for $a=0$.


Fig. 3-Variation of $\left[\left(f_{1}^{\prime}-P o^{\prime}\right) / \alpha_{2}^{2}\right) \times 10^{2}$ with $z$ for $a=-1$;


Fig. 4-Stream lines for $a=0 . K=-0 \cdot 1 \& S=03$.


Fig. 5-Variation of $\left(g_{q}\left(\alpha_{2}\right)\right.$ with $z$ for $q=0$

The stream function $\psi$ is given by (10). This equation is rewritten in the following form :

$$
\begin{equation*}
\psi^{*}=r^{* 2} f_{-1}+f_{1}+\ldots \tag{33}
\end{equation*}
$$

where $\quad \psi^{*}=\psi / R e \quad$ and $\quad r^{*}=r / R e^{1 / 2}$.

The functions $f_{-1}$ and $f_{1}$ are given by (25) and (30).


Fig. 6-Variation of ( $\mathrm{g}_{1} / \alpha_{2}$ ) with z for $a=-1$.

The streamlines for $K=-0.1$ and $S=0.3$ have been shown in Fig. 4 for $\alpha_{1}=0$ and $\alpha_{2}=-0.2$. It is of the same pattern as for Newtonian case. If we neglect the rotation perturbation term in $f_{1}^{\prime}$, the stream function $\psi$ is then simply the sum of its value for case of zero source flow and for the case of fixed disks. In this case the effect of non-Newtonian fluid parameters upto $\alpha_{i}{ }^{2}(i=1,2)$ is absent in the stream function. Therefore the streamlines are of the same form as drawn by Kreith \& Viviand ${ }^{5}$.

## ANGULAR VELOCITY

Equations (12), (26) and (31) give the angular velocity

$$
\begin{equation*}
\frac{v}{r \alpha_{2}}=\frac{1-\alpha}{2} z+\frac{1+\alpha}{2}+\frac{R e}{r^{2}}\left(g_{1} / \alpha_{2}\right) \tag{34}
\end{equation*}
$$

where $g_{1}$ is given by (31).
The angular velocity profile will differ very little from a linear profile and the difference will vanish as $r$ increases, since $\alpha_{2}$ is assumed $<\alpha$. In Fig. 5 and 6, the effect of non-Newtonian parameters on $\left(g_{1} / \alpha_{2}\right)$ for $\alpha=0$ and $\alpha=-1$, has been exhibited. Here also we note that the effect is more at $\alpha=-1$ in comparison with that at $\alpha=0$. It has been observed that the contribution of $K$ and $S$ to $\left(g_{1} / \alpha_{2}\right)$ is negligible at $\alpha=1$.

## PRESSUREDISTRIBUTION

The pressure can be obtained from (11) by neglecting the term of order Re/ $r^{2}$ or smaller. Then pressure upto second order terms in $\alpha_{i}(i=1,2)$ is given by

$$
\begin{aligned}
p & =\frac{r^{2} \alpha_{2}{ }^{2}}{20}\left[3\left(\alpha^{2}+1\right)+4 \alpha\right]-\operatorname{Re} \ln r\left[\left\{3+a^{2} \frac{263\left(\alpha^{2}+1\right)+594 a}{525}\right\}+\right. \\
& \left.+\frac{1}{4200}{a_{2}}^{2}(K+S)\left(\alpha^{2}+1\right)+744 \alpha-\frac{4}{5} a^{2}(\alpha-1)^{2}(K+S)^{2}\right]+ \\
& +\frac{1}{120} \alpha_{2}^{2}\left(z^{2}-1\right)\left\{\left(5 z^{2}-1\right)(1-\alpha)^{2}-20\left(1-\alpha^{2}\right) z\right\}+ \\
& +\frac{1}{20} \operatorname{Re}(2 K+S)\left[-z \alpha_{2}^{2}(1-\alpha)\left\{5\left(z^{2}-5\right)(\alpha+1)+\right.\right.
\end{aligned}
$$

$$
\begin{align*}
& \left.+z(1-\alpha)\left(3 z^{2}-7\right)\right\}+\left(1-z^{2}\right) \alpha_{2}^{2}(1-\alpha)\{5 z(\alpha+1)+ \\
& \left.+\frac{1}{2}(1-\alpha)\left(3 z^{2}-7\right)+3 z^{2}(1-\alpha)\right\}-20(K+S)(\alpha-1)^{2}\left(1-3 z^{2}\right) \alpha_{2}+ \\
& \left.+\frac{1}{20} \alpha_{2}^{2}(1-\alpha) z\left\{(1-\alpha)\left(20 z^{3}-12 z\right)+(60 z-20)\right\}\right]+ \text { const. } \tag{35}
\end{align*}
$$

The radial pressure distribution and the strength of the source are given by the first two terms as a function of the Taylor numbers for the upper and lower disks. The axial variation in pressure is given by the third term as a function of the axial distance from the centre plane.

The average normal force on the circular portion of the radius $r_{1}$ of the disk $z=1$, is

$$
\begin{align*}
\frac{1}{\pi r_{1}^{2}} \int_{0}^{r_{1}} 2 \pi r\left(\tau_{z z}\right)_{z=1} d r & =\frac{\phi_{1}}{2 a^{2} \rho}\left\{r _ { 1 } ^ { 2 } \left[-a_{2}^{2}\left\{\frac{3}{20}\left(\alpha^{2}+1\right)+\frac{1}{5} \alpha-\frac{5}{8}(\alpha-1)^{2}\right\}+\right.\right. \\
& \left.+\frac{1}{4} \alpha_{2}^{2}(1-\alpha)^{2}\right]-\operatorname{Re}\left(2 \ln r_{1}-1\right)-\left[3-\frac{1}{525} \alpha_{2}^{2}\right. \\
& \quad\left\{263\left(\alpha^{2}+1\right)+494 \alpha\right\}^{2}-\frac{1}{175}(K+S) \alpha_{2}^{2}\left\{4\left(\alpha^{2}+1\right)+\right. \\
& \left.\left.+31 \alpha\}+\frac{4}{5} \alpha_{2}^{2}(\alpha-1)^{2}(K+S)^{2}\right]\right\}+Q_{0} \tag{36}
\end{align*}
$$

where $Q_{0}$ is constant.
Hence the disk $z=1$ experiences suction br thrust according as

$$
\begin{align*}
& r_{1}^{2} \alpha_{2}^{2}\left[9 \alpha^{2}-38 \alpha+9\right]-8 \operatorname{Re}\left(2 \ln r_{1}-1\right)\left[-15-\frac{1}{105} \alpha_{2}^{2} .\right. \\
& .\left\{263\left(\alpha^{2}+1\right)+494 \alpha\right\}-\frac{1}{35}(K+S) \alpha_{2}^{2}\left\{4\left(\alpha^{2}+1\right)+31 \alpha\right\}+ \\
& \left.+4 \alpha_{2}^{2}(\alpha-1)^{2}(K+S)^{2}\right]>\frac{80 Q_{0} a^{2} p}{\phi_{1}} . \tag{37}
\end{align*}
$$

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## REFERENCES

1. Brbitner, M.C. \& Pohlhausan, K., "Report No. ARL-62-318", (Aerospace Research Laboratory, Wright Patterson AFB, Ohio), 1962.
2. Kreith, F. \& Peube; J.L., Compt. Rend. Acad. Sci., (Paris), 260 (1965), 5184.
3. Peibe, J.L. \& Kritte, F., J. de Mec., 5 (1966), 261.
4. Pelech, I. \& Shapiro, A., J. Appl. Mech., 31, No. 4. Trans. ASME, 86, Series E (1964), 1777.
5. Kreitit, F. \& Viviand, H., J. Appl. Meoh., Trans. ASME, 34 (1967), 541.
6. Mellor, G.L., Chapple, P.J. \& Stokes, V.K., J. Fluid Mech., 31 (1968), 95.
7. Rajvanshi, S.C., Def. Sci. J., 19 (1969), 39.
8. Colmman, B.D. \& Noll, W., Arch. Ratl. Mech. Anal., 2 (1958), 197.
9. Casal, P., Compt. Rend. Acad, Sci. (Paris), 280 (1950), 178,
