# IMPULSIVE DEBOOST FOR MAXIMUM AND MINIMUM ATMOSPHERIC ENTRY ANGLES

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Deboost of rocket vehicles initially moving in elliptic orbits for maximum and minimum atmospheric entry angles is analysed. It is shown that in general with specified retrofire velocity impulse and entry altitude, maximum entry angle is obtained when retrofire impulse is applied tangentially at the apogee whereas minimum entry angle occurs when retrofire impulse is applied tangentially at the perigee. Existence conditions for only maximum or minimum or both or neither maximum nor minimum entry angles have also been investigated.

The problem of maximizing the atmospheric entry angle for specified retrofire impulse in case of a rocket vehicle moving initially in elliptic orbit is analysed in reference 1. The results of the two numerical examples worked out therein lead to the conclusion that maximum entry angle at a given entry altitude occurs for tangential retrofire impulse at the apogees. But the conclusion derived there in from numerical cases lacks generality unless an analytical proof is given.

The object of this paper is to show that (i) the aforementioned conclusion is a general one, (ii) to analyse the case when the mission is impulsive deboost for minimum atmospherie entry angle with given retrofire impulse at an assigned entry altitude. In case (ii) it is shown that the retrofire impulse should be applied tangentially to the rocket at the perigee of the elliptic orbit in which the rocket was moving prior to deboost. Conditions under which either maximum or minimum or no extreme entry angle or both maximum and minimum entry angles will occur have also been derived.

#### ANALYSIS.

Let the equation of the elliptic orbit in which the rocket is moving initially be

$$l = r \left( 1 + e \cos \theta \right) \tag{1}$$

where l is semi-latus rectum, e is eccentricity of the orbit and  $r,\theta$  represent radius vector and true anomaly respectively. If  $\gamma$  is angle between velocity and the local horizontal and suffixes 1 and E represent conditions just after the retrofire impulse and at the entry point respectively (Fig. 1), it is shown in reference 1 that the atmospheric entry angle  $\gamma_E$  at a radial distance  $r_E$  from the force centre is given by

$$\cos \gamma_E = \frac{\left[ (\mu l)^{\frac{1}{2}} - \triangle V \, r_0 \cos \left( \gamma_0 + \beta \right) \right]}{r \left[ \mu \left( \frac{2}{r_E} - \frac{1 - e^2}{l} \right) - 2\triangle V \cdot V_0 \cos \beta + (\triangle V)^2 \right]^{\frac{1}{2}}} \tag{2}$$

where  $\mu$  is gravitational parameter,  $\triangle V$  is the retrofire impulsive velocity decrement applied to the rocket at the point  $(r_0, \theta_0)$  of the initial orbit at an alignment angle  $\beta$  and  $\gamma_0$ ,  $V_0$  are the values of  $\gamma$  and velocity of the rocket vehicle at the point  $(r_0, \theta_0)$  prior to the application of the velocity impulse.

 $\gamma_0$  and  $V_{\bullet}$  can be expressed as

$$\tan \gamma_0 = \frac{e \sin \theta_0}{1 + e \cos \theta_0} \tag{3}$$

$$V_0 = \left[ \frac{\mu}{l} \left( 1 + e^2 + 2e \cos \theta_0 \right) \right]^{\frac{1}{2}} \tag{4}$$

For specified  $\triangle V$  and  $r_E$ , by virtue of (1), (3) and (4),  $r_E$  is a function of two variables  $\beta$  and  $\theta_0$  and the equations giving the values of  $\beta$  and  $\theta_0$  which after substituting in (2) will give extreme values of  $r_E$ , are

$$\dot{r}_0 \sin \left(\gamma_0 + \beta\right) \left[ (\mu l)^{\frac{1}{2}} - \triangle V \, r_0 \cos \left(\gamma_0 + \beta\right) \right] = V_0 r_E^2 \cos^2 \gamma_E \sin \beta \tag{5}$$

$$r_0 \left[ (\mu l)^{\frac{\pi}{2}} \triangle V \ r_0 \cos(\gamma_0 + \beta) \right] \left[ \mu \left( e + \cos \theta_0 \right) \sin \left( \gamma_0 + \beta \right) - r_0 V_0^2 / \sin \theta_0 \cos \left( \gamma_0 + \beta \right) \right] \\ = \mu V_0 r_2 \cos^2 \gamma_E \cos \beta \sin \theta_0 \cdot (6)$$

Equations (5) and (6) give

$$\tan \beta = \frac{e \sin \theta_0 \left(\frac{l}{r_0}\right)^{\frac{1}{2}}}{\frac{l}{r_0} \left[2 \mp \left(\frac{l}{r_0}\right)^{\frac{1}{2}}\right] - (1 - e^2)}$$
(7)

Using (1), (3) and (4), (7) can be written as

$$\tan \beta = \frac{\sin \gamma_0}{V_0 \left(\frac{r_0}{\mu}\right)^{\frac{1}{2}} \mp \cos \gamma_0} \tag{8}$$

Equation (8) gives

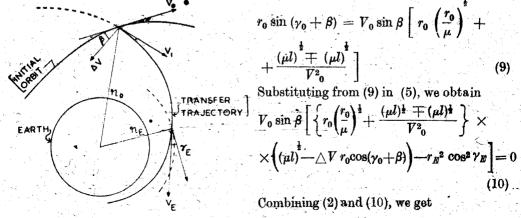


Fig. 1-Transfer geometry.

$$V_0 \sin \beta \left[ \left\{ r_0 \left( \frac{r_0}{\mu} \right)^{\frac{1}{2}} + \frac{(\mu l)^{\frac{1}{2}} \mp (\mu l)^{\frac{1}{2}}}{V_0^2} \right\} \left\{ \mu \left( \frac{2}{r_w} - \frac{1 - e^2}{l} \right) + (\triangle V)^2 - 2\triangle V. V_0 \cos \beta \right\}$$

$$- (\mu l)^{\frac{1}{2}} - \triangle V r_0 \cos (\gamma_0 + \beta) \right] = 0$$

$$(11)$$

MAXIMUM AND MINIMUM ENTRY ANGLES

Equation (11) gives

either

$$(i) \quad V_0 \sin \beta = 0 \tag{12}$$

or

(ii) 
$$(\mu l)^{\frac{1}{2}} - \triangle V \cdot r_0 \cos (\gamma_0 + \beta)$$

$$= \left\{ r_0 \left( \frac{r_0}{\mu} \right)^{\frac{1}{2}} + \frac{(\mu l)^{\frac{1}{2}} \mp (\mu l)^{\frac{1}{2}}}{V_0^2} \right\} \cdot \left\{ \mu \left( \frac{2}{r_E} - \frac{1 - e^2}{l} \right) + (\triangle V)^2 - 2\triangle V \cdot V_0 \cos \beta \right\}$$
(13)

Equation (13) gives relation between  $\beta$  and  $\theta_0$  which differs from (7). Therefore  $\beta$  and  $\theta_0$  satisfying (5) and (6) cannot satisfy (13) for arbitrary choice of  $\triangle V$  and  $r_E$  and hence (13) is invalid and therefore (12) holds good which gives  $\beta = 0$ . Substitution of  $\beta = 0$  in (7) gives  $\theta_0 = 0$  or  $\pi$ . Since  $\gamma_E$  is a continuous and derivable

function of  $\beta$ ,  $\theta_0$  in the domain  $-\frac{\pi}{2} < \beta \le \frac{\pi}{2}$  and  $0 \le \theta_0 \le 2\pi$ , therefore at

 $(\beta = 0, \theta_0 = 0)$  and  $(\beta = 0, \theta_0 = \pi)$ ,  $\gamma_E$  attains its extreme values. To decide which of the two points corresponds to the maximum and which to the minimum value of  $\gamma_E$ , we get from (2)

$$\cos \gamma_E \atop (\beta = 0, \theta_0 = 0) = \frac{(\mu l)^{\frac{1}{2}} - \triangle V. r_p}{r_E \left[ \xi - 2 \triangle V. V_p \right]^{\frac{1}{2}}}$$
(14)

and

$$\cos \gamma_{E} = \frac{(\mu l)^{\frac{1}{2}} - \triangle V \cdot r_{a}}{r_{E} \left[ \xi - 2 \triangle V \cdot V_{a} \right]^{\frac{1}{2}}}$$
(15)

where

$$\xi = \mu \left( \frac{2}{r_E} - \frac{1 - e^2}{l} \right) + (\triangle V)^2$$

and subscripts p, a represent values at the perigee and apogee respectively of the initial orbit.

Now since  $r_p < r_{\widehat{\alpha}}$  and  $V_p > V_{\alpha}$ , therefore from (14) and (15) for specified  $\triangle V$  and  $r_E$ , we have

$$\begin{array}{cc} \cos \gamma_E & > \cos \gamma_E \\ (\beta=0, \ \theta_0=0) & (\beta=0, \ \theta_0=\pi) \end{array}$$

which gives

$$\begin{array}{cccc} \gamma_E & < & \gamma_E \\ (\beta=0, \ \theta_0=0) & (\beta=0, \ \theta_0=\pi) \end{array}$$

Thus  $\gamma_E$  attains its maximum value at the point  $(\beta = 0, \theta_0 = \pi)$  and minimum value at  $(\beta = 0, \theta_0 = 0)$ . The minimum and maximum value of  $\gamma_E$  are given by

(14) and (15) respectively. Therefore we arrive at the conclusion that for specified  $\triangle V$  and  $r_F$ , atmospheric entry angle is maximum when  $\triangle V$  is applied tangentially at the apogee and minimum when  $\triangle V$  is applied tangentially at the perigee of the initial orbit.

EXISTENCE CONDITIONS FOR EXTREME ENTRY ANGLES
Equations (14) and (15) can be transformed into

$$\frac{\cos \gamma_E}{(\beta=0, \, \theta_0=0)} = \frac{l}{r_E \left[ (1+e)^2 + \frac{2\mu \left(\frac{1}{r_E} - \frac{1+e}{l}\right)}{\left[\left(\frac{\mu}{l}\right)^{\frac{1}{2}} - \frac{\triangle V}{1+e}\right]^2} \right]^{\frac{1}{2}}}$$
(16)

and

$$\frac{\cos \gamma_E}{(\beta = 0, \, \theta_0 = \pi)} = \frac{l}{r_E \left[ (1 - e)^2 + \frac{2\mu \left( \frac{1}{r_E} - \frac{1 - e}{l} \right)}{\left[ \left( \frac{\mu}{l} \right)^{\frac{1}{2}} - \frac{\triangle V}{1 - e} \right]^2} \right]^{\frac{1}{2}}} \tag{17}$$

For existence of minimum  $\gamma_E$ , (16) gives

$$(1+e)\left(\frac{\mu}{l}\right)^{\frac{1}{2}}\left[1-\left(\frac{2r_E}{l+r_E(1+e)}\right)^{\frac{1}{2}}\right] \leqslant \triangle V \leqslant (1+e)\left(\frac{\mu}{l}\right)^{\frac{1}{2}}\left[1+\left(\frac{2r_E}{l+r_E(1+e)}\right)^{\frac{1}{2}}\right]$$
(18)

Similarly for existence of maximum  $\gamma_E$ , (17) gives

$$\left(\frac{\mu}{l}\right)^{\frac{1}{2}}(1-e)\left[1-\left(\frac{2r_{E}}{l+r_{E}(1-e)}\right)^{\frac{1}{2}}\right] \leqslant \triangle V \leqslant \left(\frac{\mu}{l}\right)^{\frac{1}{2}}(1-e)\left[1+\left(\frac{2r_{E}}{l+r_{E}(1-e)}\right)^{\frac{1}{2}}\right] (19)$$

Thus if (18) is satisfied and (19) is not satisfied, only minimum  $\gamma_E$  will exist and vice versa. But if (18) and (19) both are satisfied, both maximum and minimum  $\gamma_E$  will exist and if none of them is satisfied, no extreme will exist.

## CONCLUSIONS

For a rocket vehicle moving initially in an elliptic orbit,

- (i) Maximum atmospheric entry angle at a given entry altitude occurs by tangentia retrofire impulse at the apogee.
- (ii) Minimum atmospheric entry angle at a given entry altitude occurs by tangentia retrofire impulse at the perigee.
- (iii) Existence of only maximum or minimum or both or neither maximum nor minimum atmospheric angles depend upon (18) and (19).

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#### REFERENCE

1 SRIVASTAVA, T. N. & Nagpal, O. P., Def. Sci. J., 19 (1969), 183.